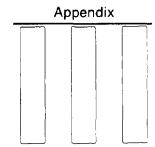
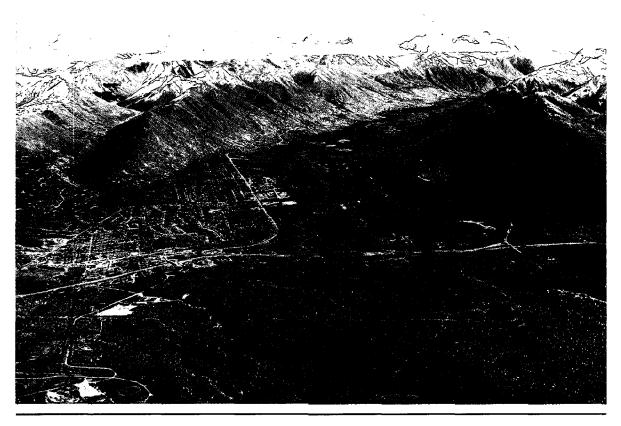
## TASK 3 FLOUR WATER TREATMENT STUDY



Eagle River Water Resource Study



Municipality of Anchorage Water and Sewer Utilities

00 00011

TD 412 .E34 1981 no.3

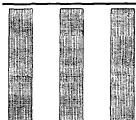
The work with the sold of the sold with the sold of th

IILL

December 1981

# TASK 3 FLOUR WATER TREATMENT STUDY

Appendix



Eagle River Water Resource Study

Municipality of Anchorage Water and Sewer Utilities

US Department of Commerce NOAA Coastal Services Center Library 2234 South Hobson Avenue Charleston, SC 29405-2413

CH2M#HILL

December 1981



This report was prepared under the supervision of a registered professional engineer.

The preparation of this report was financed in part by funds from the Office of Coastal Zone Management, National Oceanic and Atmospheric Administration, U.S. Department of Commerce, administered by the Diversion of Community Planning, Alaska Department of Community and Regional Affairs.



To pursue the recommendations for further study that were prescribed in the <u>Metropolitan Anchorage Urban Study</u>, completed by the U.S. Corps of Engineers in 1979, the <u>Municipality</u> of Anchorage engaged CH2M HILL to conduct the Eagle River Water Resource Study. The purpose of the study is to investigate the potential sources of water supply from the Eagle River Valley. The original scope of the study comprised four tasks:

Task 1	Well Drilling Program
Task 2	Preliminary Damsite Investigation
Task 3	Flour Water Treatment Study
Task 4	Transmission Main Design

Task 5, Eklutna Lake Alternative Water Source Evaluation, was added to the scope after the completion of the first four tasks.

The report for each task is bound separately and is an appendix to the Executive Summary of the entire study. This Appendix III is the report for Task 3, Flour Water Treatment Study.

## ACKNOWLEDGMENTS

We wish to express our appreciation to the Anchorage Water and Sewer Utilities staff for their contributions at the weekly meetings, updating of task scopes, and overall administrative assistance.

Also, we thank Eklutna, Inc., for providing pertinent information at the weekly meetings and ready access to its property.

The objectives of Task 3 are to (1) determine whether surface water from the Eagle River can be treated by conventional processes to remove glacial rock flour in order to meet current drinking water standards and (2) estimate costs for such treatment.

Field and laboratory testing indicated that Eagle River water is treatable. Treatment facilities will require two different seasonal treatment processes that can be provided in a single water treatment plant. Transition between processes would occur in June and September correlating with melting of the glaciers at the river's headwaters.

The recommended treatment processes are: (1) flocculation, sedimentation, high-rate filtration, and disinfection for the high-turbidity, glacial melt period; and (2) coagulation, high-rate filtration, and disinfection for the low-turbidity period during the colder months.

To provide flexibility and to meet increasing water demands, the treatment plant could be constructed in three equal increments of 23.33 mgd each until the full capacity of 70 mgd was reached. Additions could be made when needed with little disruption to continuing operation of existing facilities. Capital costs and annual operation and maintenance costs were estimated in January 1981 dollars for a 23.33-mgd and a 70-mgd plant. These estimated costs are \$17.4 million (capital) and \$1 million (operation and maintenance) for a 23.33-mgd plant and \$41.4 million (capital) and \$2.7 million (operation and maintenance) for a 70-mgd plant.

Prior to starting final design but after selection of Eagle River surface water as the source for additional water supply, we recommend the following:

- o Pilot treatment plant tests for a full year, using at least a 1-mgd plant, to determine applicable process design criteria. This testing program should address iron, color, and turbidity removal; chemical dosages required over the full range of raw water parameters; filtration rates and media selection; and effectiveness of the recommended treatment processes.
- o Investigation of disinfection alternatives to identify their trihalomethane formation potential (formation of potentially carcinogenic substances during the disinfection process).

- o Identification of sludge disposal alternatives and the associated cost research.
- o Selection of a treatment plant site.
- Groundwater quality analysis and monitoring program for the old Eagle River dump.



Alum Metallic salt, aluminum sulfate, coag-

ulant used in removal of turbidity

from water

Coagulation A chemical process for combining

particles into larger aggregates

Degrees C Degrees centigrade

7° C = 45° F (Fahrenheit) and 20° C =

68° F

**EPA** United States Environmental Protection

Agency

Flocculation The process of gentle mixing following

coagulation so that particles come in contact with one another, aggregating or growing into larger more dense

particles that settle readily

Flour Material ground by glaciers

Jar Testing A bench-scale procedure using multiple

stirrers to compare coagulation and settling results in beakers having

varying coagulant dosages

million gallons per day mgd

milligrams per liter mq/1

Unit Micron of measure equalling one

thousandth of a millimeter

Nephelometric Turbidity Unit - unit NTU

for measuring turbidity

Sedimentation Process by which coagulated

> suspended matter separates from the water by subsidence and deposition

THM

Organic compounds formed when certain (trihalomethane)

natural organic compounds (particularly humic acids) come in contact with chlorine. These compounds are thought

to cause cancer in animals.

Turbidity A measurement of water clarity by the

amount of particulate matter in the

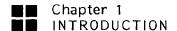
sample

#### CONTENTS

	•	Page
	Preface	iii
	Acknowledgments	V
	Summary and Conclusions	vii
	Definition of Terms	ix
1	Introduction Background Purpose and Scope Site Description Limitations	1-1 1-1 1-5 1-6 1-6
2	Data Collection and Evaluation Sampling Site Equipment Tests	2-1 2-1 2-1 2-1
3	Treatment Requirements and Recommendations Treatment Requirements Treatment Processes Treatment Plant Alternative Treatment Methods	3-1 3-1 3-2 3-4 3-8
4	Cost Estimate	4-1
5	Bibliography	5-1
	bit A. USGS Water Quality Data	

### **TABLES**

		Page
2-1	Chemical Analysis, Summer 1980	2-2
3-1	Water Quality Standards and Raw Eagle River Quality	3-1
4-1	Estimated Project Costs	4-1
FIGUR	ES	
1-1	Vicinity Map	1-2
1-2	Projected Water Demand Increase 1980-2025	1-3
2-1	Air and Water Temperature	2-3
2-2	Turbidity	2-4
2-3	Turbidity vs. Dissolved and Suspended Solids	2-6
2-4	рН	2-7
2-5	Hardness and Alkalinity	2-8
2-6	Coagulation of Water With High Turbidity	2-9
2-7	Settled Water Turbidity vs. Alum Dosage	2-10
2-8	Settled Water Turbidity vs. Alum Dosage at Various Water Temperatures	2-12
2-9	Settled Water Turbidity vs. Settling Time at Various Water Temperatures	2-13
2-10	Settled Water Turbidity vs. Temperature and Settling Time	2-14
3-1	Treatment Process Options	3-3
3-2	Typical Plant Flow Schematic	3-5
3-3	Preliminary Plant Layout	3-6



#### BACKGROUND

The population and, thus, the water supply needs of the metropolitan Anchorage area are growing rapidly. Presently, surface water from Ship Creek and groundwater wells in the Anchorage Bowl supply most of the municipality's water. However, if present growth trends continue, these sources will not meet future needs.

In 1974 the United States Congress authorized the U.S. Army Corps of Engineers to perform the Metropolitan Anchorage Urban Study (MAUS), which was completed in 1979. The purpose of the MAUS was "to evaluate the adequacy of the developed water supply in the metropolitan Anchorage area, to determine future water demands, to assess sources for water supply development, and to formulate water supply plans to meet the increased future demand" (U.S. Army Corps of Engineers, 1979). The MAUS study area comprised the Anchorage Bowl and the area northeast to the town of Eklutna (Figure 1-1).

The projected future water demand increases, determined in the MAUS, are shown in Figure 1-2. It is expected that by the year 2025 an additional 81.5 million gallons per day (mgd) of water will be needed to meet the increased demands in the area.

The MAUS report identified many potential sources of supply: Eagle River Valley groundwater; Anchorage Bowl groundwater; and surface water from Campbell Creek, Ship Creek, Eagle River, and Eklutna Lake. Two plans were recommended by MAUS for future study. Plan IV, which ranked first environmentally and socially, included a combination of supply from Ship Creek, Anchorage Bowl groundwater, and Eklutna Lake. Plan VI, which ranked first on an economic basis, included an increased supply from Ship Creek, winter diversion from Eagle River, further development of Anchorage Bowl groundwater, and exploration for Eagle River Valley groundwater.

To implement portions of these plans, the Municipality increased the water supply from within the Anchorage Bowl by recently constructing a 36-inch supply main to its water treatment plant from the military diversion facility on Ship Creek. Future developments are expected to include new wells to increase groundwater supply and the expansion of the capabilities of the plant that treats Ship Creek water. However, rapidly growing demands in Anchorage will require development of a new source outside the Anchorage Bowl within the next 10 years. The Eagle River-Chugiak-Eklutna area, northeast of Anchorage, needs a new source now.

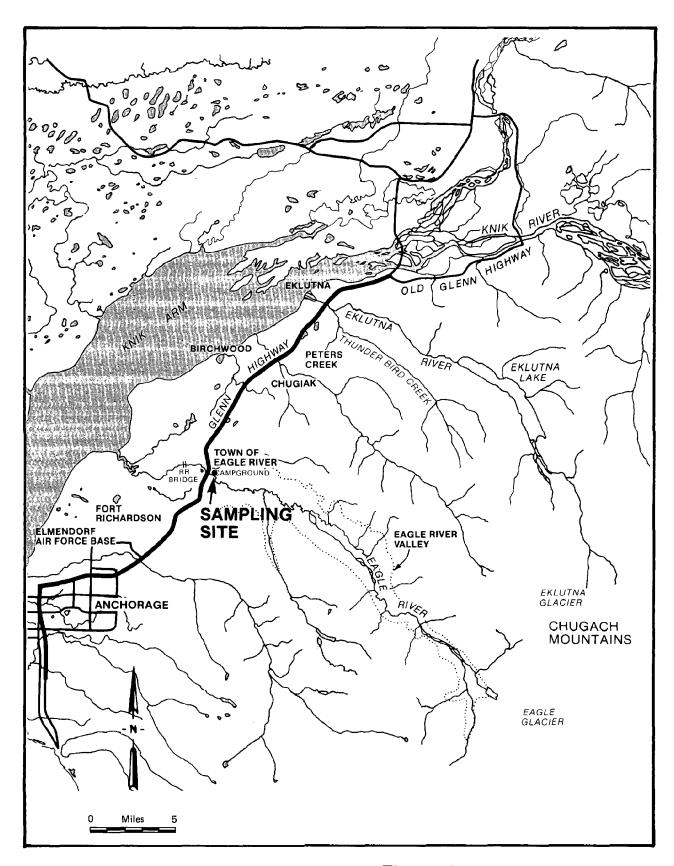
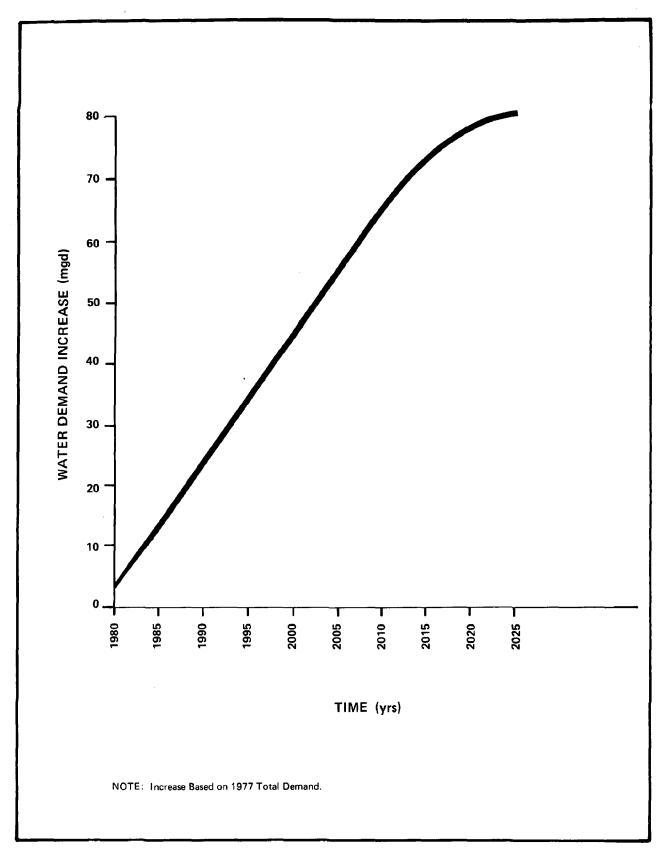


Figure 1-1 Vicinity Map



SOURCE: U.S. Corps of Engineers. 1979.

Figure 1-2 Projected Water Demand Increase 1980-2025

As a result of the MAUS findings, the Municipality decided to investigate potential sources outside the Anchorage Bowl that could supply 70 mgd of water. On the basis of the MAUS population projection, this diversion would satisfy the demands of the entire study area through the year 2012. The future increases in water supply capacity that are expected to be developed within the Anchorage Bowl will delay the need for the full 70-mgd capacity of the new water source outside the Bowl until approximately the year 2020 or later.

The Eagle River Valley is one possible source of water from outside the Anchorage Bowl that was suggested in the MAUS, Plan VI. To investigate the potential of this valley to supply the 70-mgd requirement, the Municipality engaged CH2M HILL to conduct the Eagle River Water Resource Study. The original scope of the study comprised four separate tasks:

- o Task 1, a well drilling program to study the feasibility of developing the Eagle River Valley as a groundwater source
- Task 2, a preliminary damsite investigation to determine the feasibility of developing the Eagle River as a surface water source
- o Task 3, an investigation of the suitability of conventional treatment processes for removal of glacial rock flour from the Eagle River water
- o Task 4, a preliminary design of a pipeline to transport groundwater or surface water from the Eagle River Valley to Anchorage

Each task was conducted independently.

The results of the first four tasks clearly indicate that a substantial dam and reservoir are required to develop Eagle River as a water source. Before committing itself to this dam and reservoir project, the Municipality of Anchorage increased the study scope to include Task 5, Eklutna Lake Alternative Water Source Evaluation. The purpose of Task 5 was to analyze the capability of Eklutna Lake to supply the 70 mgd of water to the area. Eklutna Lake is included in Plan IV of the MAUS. The lake is 30 miles northeast of downtown Anchorage and 16 miles northeast of the Eagle River (Figure 1-1).

The report for each task appears as an appendix to the Executive Summary of the entire study. This Appendix III is the report for Task 3, Flour Water Treatment Study.

#### PURPOSE AND SCOPE

The objective of Task 3 is to investigate the suitability of the Eagle River as a potable water supply source, especially during the summer glacial melt period. It is intended to complement the MAUS and to augment water quality data collected by the United States Geological Survey (USGS) between 1948 and 1973.

If the 70-mgd source of water for the Municipality of Anchorage is to come from Eagle River surface water (assuming it can be made potable), a plant to treat this water should be located near the river. This will allow potable water to be pumped south to the Anchorage Bowl and north to various communities as far away as Eklutna (Eagle River, Chugiak, Birchwood, Peters Creek, and Eklutna). Initially, when demands are still low, untreated water could be pumped to the existing Municipal Water Treatment Plant. However, it is likely that the Eagle River treatment plant would be constructed when the dam (Appendix II of this study) is constructed so the areas north can be served. To provide flexibility and to meet increasing demands, the treatment plant could be constructed in stages.

This appendix contains the following:

- o Results and evaluations of field and laboratory tests
- o Identification of treatment criteria and the best treatment processes for both the summer glacial melt period and the winter clear water periods
- o Estimated project and annual operation and maintenance costs for a treatment plant suitable for operation of the recommended processes

The Municipality of Anchorage suggested that we study flour concentration, exchange capacity, particle size, mineral concentration, solution characteristics, and treatment agents and methods. These suggested areas of the study, except for the exchange capacity and particle size, influence the treatment required to produce potable water and were considered throughout this task. Exchange capacity relates to ion exchange, which is a common process in water softening. Eagle River water is naturally soft and does not require softening. Particle size, though of interest, does not relate directly to its removal. Particle size distribution was measured but is not considered as having a direct bearing on either the jar tests performed or the treatment conclusions resulting from these tests.

Data were collected during the entire glacial melt period, June through September 1980. During this period, data were gathered regularly, and observations were made of variations in river water quality.

#### SITE DESCRIPTION

The Eagle, River, situated about 10 miles northeast of Anchorage, is fed primarily by the Eagle Glacier at the upper end of the Eagle River Valley (Figure 1-1). During the summer, melt water from the glacier contributes to high flows. This melt water contains glacial rock flour, which produces high turbidity in the water. In the winter months when the glacier is frozen, streamflow and turbidity are low. Its turbidity makes the Eagle River water unsuitable for drinking. A method for reduction of turbidity must be determined before the Eagle River can be identified as a potential drinking water source.

#### LIMITATIONS

This report was prepared for the use of the Anchorage Water and Sewer Utilities for specific application to the Eagle River Water Resource Study, Flour Water Treatment Study, in accordance with generally accepted engineering practice. No other warranty, expressed or implied, is made. In the event of any changes to the conditions considered under this study, the conclusions and recommendations contained in this report will not be considered valid unless the changes are reviewed and the conclusions or recommendations are modified or verified in writing by CH2M HILL.

The purpose of this task is to investigate whether conventional treatment processes can remove glacial rock flour from Eagle River water. No design criteria were developed. The treatment concepts presented in this report are believed to be workable but are not refined enough for incorporation into a final design. Additional investigations, such as pilot testing, will be required prior to final design.

#### SAMPLING SITE

All samples for testing were collected from the right bank of the Eagle River immediately upstream of both the Glenn Highway bridge and the confluence of Meadow Creek with the Eagle River (Figure 1-1). This site was readily accessible during all weather conditions and permitted an undisturbed location to park the mobile laboratory. Because the river at this location is extremely turbulent; grab sampling from the river bank was considered as representative of the entire river. This was confirmed by taking samples upstream, near the center of the river, and measuring turbidity.

Other sites further upstream were considered for regular sampling but were eliminated because they were less convenient and required permits for access. No significant tributaries enter the river between the sampling site and either of the two prospective damsites, identified in Appendix II of this study.

#### EQUIPMENT

The mobile laboratory was equipped with a four-paddle stirrer, a Hach Model DREL turbidimeter, a pH meter, and miscellaneous other glassware and equipment for titrating.

#### TESTS

The testing started on June 11, 1980, and continued into September, covering the entire rock flour, glacial melt period.

Temperature, pH, hardness, alkalinity, and turbidity tests were performed at the sampling point. Also, jar testing was used to determine optimum coagulant dosage, effects of rapid and slow mixing, and floc settling rate. These tests were conducted daily until repeatable results to primary variables were established. Testing frequency was then reduced to 3 days per week unless significant changes in weather or stream condition occurred.

In addition to on-site testing, samples were collected and transported to an off-site laboratory for particle size analysis and other routine chemical and physical analyses. These tests were performed bimonthly throughout the testing period.

Results of the on-site and off-site tests are shown on Table 2-1. Additional Eagle River raw water quality data, obtained between January and June 1981, is contained in Exhibit B at the end of this appendix.

Table 2-1 CHEMICAL AND PHYSICAL ANALYSES SUMMER 1980

•	Dates							
	7-23	7-28	8-8	8-15	8-25	8-29	9-5	9-16
Ca (mg/l)	12	11	12	13	19	19	21	12
Fe (mg/l)	4.4	4.6	1.6	1.0	0.5	1.3	0.4	4.2
Mn (mg/l)	0.07	0.08	0.04	< 0.05	<0.05	0.06	< 0.05	0.07
Si (mg/l) SiO <sub>2</sub> (mg/l)	$\frac{13.2}{28}$	$\frac{14.4}{30.9}$	8.8	6.8	<u>-</u> 5.1	<del>-</del> <del>2.7</del>	2.8	$\frac{10.4}{22.3}$
Nitrate (mg/l)	0.26	< 0.10	0.18	0.26	0.17	0.19	0.21	0.67
Sulfate (mg/l)	8.4	< 1	4.5	0.5	7.5	9.5	9.0	3.5
Total Dissolved Solids (mg/l)	137	79	99	71	92	110	105	85
Turbidity (NTU) Suspended Solids (mg/l)	160 242	300 400	180 232	80 99	35 44	26 18	12 6.4	361
Hd CACO <sub>3</sub> (mg/I)	44	-	43	55	64	70	78	52
Alkalinity as CaCO <sub>3</sub> Bicarb. HCO <sub>3</sub> (mg/l) Carb. CO <sub>3</sub> (mg/l)	52 0	60 0	51 0	97 0	110 0	84 0	88 0	55 0
Conductivity (umhos)	100	84	92	96	120	140	165	100
'Color (cu)	10	30	> 70	50	45	35	30	30
Chloride (mg/l)	2	30	8	5	2	2	< 1	<1

#### Temperature

Figure 2-1 shows a plot of both air and river water temperatures throughout the test period. While air temperatures were generally in the 15-degree- to 20-degree-C range, water temperatures held fairly constant at 6 degrees to 7 degrees C.

During the test period there was a general relationship between air and water temperature. This is illustrated by the drop in both air and water temperature between August 29 and September 8.

#### Turbidity

Turbidity ranged from 30 to 400 NTU, with the normal at about 150 NTU (Figure 2-2). Turbidity in the Eagle River is directly

Eagle River Water Temperature 1980 July 15 June 200 TEMPERATURE (°C)

Figure 2-1 Air and Water Temperature

Figure 2-2 Turbidity

linked to air temperature and rate of melt of the glaciers feeding the river. The river appears greyish in color, which is typical of the rock flour solids that create the turbidity.

Periodically, samples were analyzed for both dissolved and suspended solids. Occurrence of these solids was plotted against turbidity (Figure 2-3). This plot indicates a rough correlation between turbidity and suspended solids, a turbidity of 75 NTU equaling approximately 100 mg/l of suspended solids. Dissolved solids remain more or less constant regardless of turbidity or suspended solids.

Suspended solids particles that cause turbidity were analyzed for size distribution. The six samples analyzed showed that 90 percent of the particles were smaller than 2 microns, and 87 percent were larger than 0.5 micron. The particle count mean averaged 0.86 micron.

The data from tests taken during the summer of 1980 closely resemble water quality data gathered by the USGS during the period 1948 to 1973. (The USGS data are included as Exhibit A at the end of this report.) Suspended solids measurements and turbidity generally agree with historic data; however, the previous high suspended solids loadings of 1,200 to 1,400 mg/l were not observed. Our maximum observation was 400 mg/l. Either the high loadings did not occur this year or they were missed, even though a conscious effort was made throughout the summer to take samples when changes in temperature, runoff, and rainfall were observed.

#### рΗ

The pH of Eagle River water was fairly constant, generally between 7.3 and 7.5. This information is plotted in Figure 2-4.

#### Alkalinity and Hardness

Alkalinity and hardness vary seasonally and seem to correlate with turbidity. Both alkalinity and hardness decrease during the summer months, which are associated with higher streamflow and turbidity. Alkalinity varies from 50 to 60 mg/l in the winter to 30 to 45 mg/l in the summer. Similarly, hardness varies from 70 to 80 mg/l during the winter to 40 to 50 mg/l in the summer. Both the alkalinity and hardness of the Eagle River water during the sampling period are expressed in milligrams per liter as CaCO in Figure 2-5.

#### Jar Testing

Jar testing is a bench-scale test that gives insight into full-scale coagulation and settling processes. The primary purpose for jar testing in this task was to determine how different coagulant

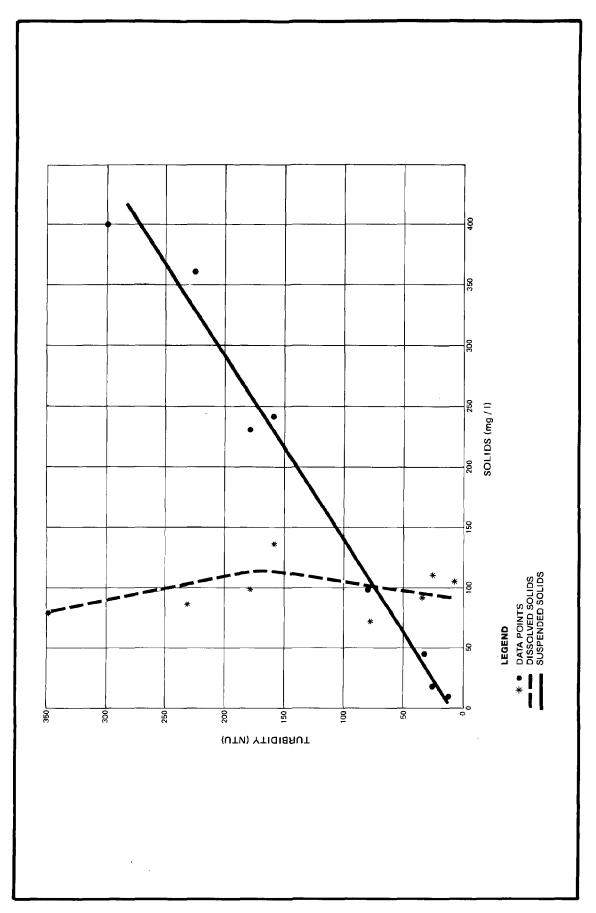


Figure 2-3 Turbidity vs Dissolved and Suspended Solids

Figure 2-4 pH

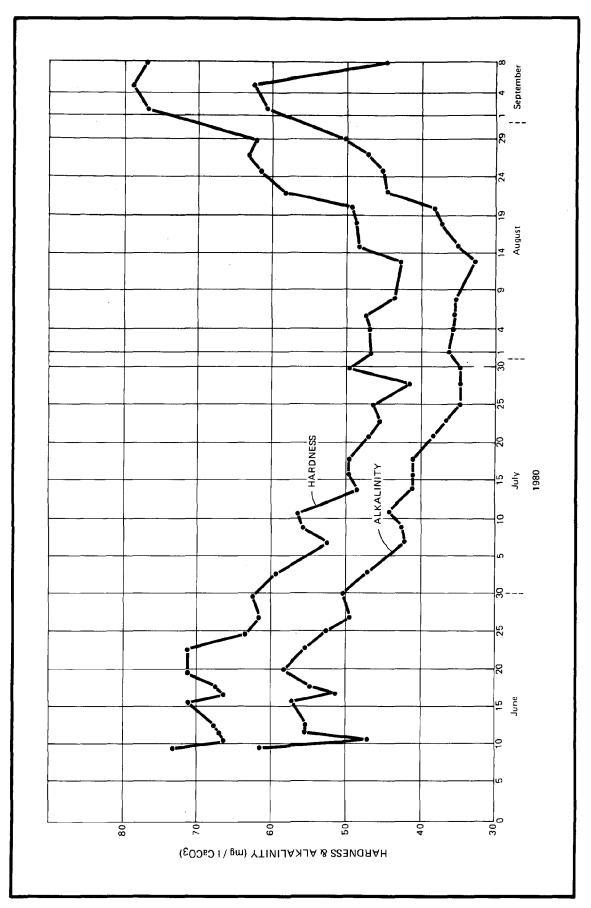


Figure 2-5 Hardness and Alkalinity

(alum) dosages reacted with the range of raw water quality during the highly turbid glacial melt period. The effects of changing water temperatures, rapid and slow mixing rates, and rapid and slow mixing durations were then investigated to refine the treatment requirements of the Eagle River water.

Initial jar testing showed that two separate alum dosage ranges achieved coagulation and clarification within a broad range of alum dosage. Figure 2-6 shows alum dosage plotted against turbidity after mixing and settling. The plot shows four distinct zones that occur frequently in treating highly turbid river water. When proceeding from left to right the zones can be described as follows: (1) insufficient alum, thus no coagulation, (2) effective alum dosage that achieves coagulation-clarification through destabilization of turbidity particles, (3) another zone of ineffective coagulation, and (4) a second zone of effective coagulation-clarification, this time resulting by adsorption and enmeshment of turbidity particles.

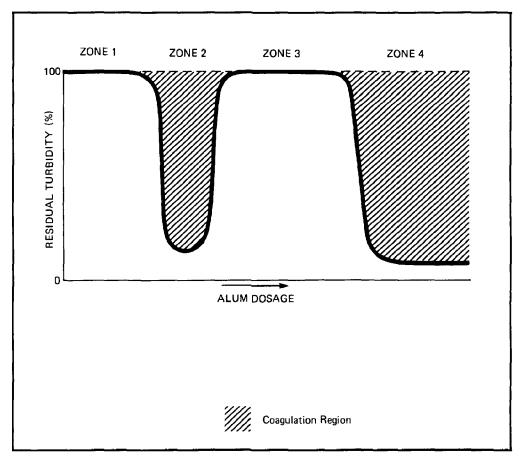


Figure 2-6 Coagulation of Water With High Turbidity

Plant-scale operation would use Zone 2 rather than Zone 4 because less alum is used and a reduced volume of sludge is produced. Subsequent testing focused on this lower dosage zone to establish how dosage requirements varied with changing river turbidity and temperature. The optimum alum dosage for the summer's test program was between 10 and 15 mg/l.

The jar testing results showed that turbidity can be removed effectively through use of coagulation, flocculation, and sedimentation. The settled water produced from these procedures has a turbidity of 10 NTU or less for raw river water temperatures between 3 degrees and 7 degrees C regardless of turbidity. Figure 2-7 shows a typical plot of alum dosage against turbidity after settling.

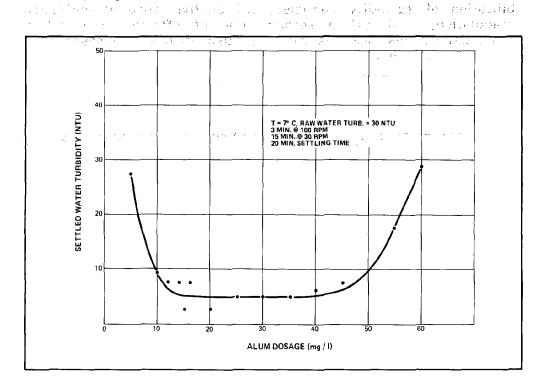


Figure 2-7
Settled Water Turbidity vs
Alum Dosage

Once the optimum dosage of 10 to 15 mg/l of alum was established, testing then turned to identifying whether an increase in water temperature above the natural river temperature would have a significant effect on coagulation, flocculation, and sedimentation (Figures 2-8, 2-9, and 2-10). In general, settling occurred more rapidly as the water temperature increased; however, the end

turbidity was the same. There is a possibility that river water could be preheated as it enters the treatment plant by waste heat energy from a future fossil-fuel-fired electric power plant being considered.

Additional testing established, in a general sense, the effect of varying either or both rapid mixing and slow mixing on floc formation and settling characteristics. Rapid mixing performed best with the stirrer set at 90 rpm for 3 to 5 minutes, and the slow mixing appeared to be most effective at 30 rpm for 12 to 15 minutes. Using optimum rapid and slow mixing, the best observed settled water characteristics resulted after 20 to 25 minutes. No attempt was made to correlate the jar stirrer with plant-scale mixing equipment.

Because the alum dosage requirement was so low, little subsequent testing was done using polymers as a substitute coagulant or as a coagulant aid.

Use of alum as a coagulant has a side effect of lowering the pH of the water, which often increases the corrosiveness of the water to piping systems and household plumbing. Because the decrease of the pH using 10 to 15 mg/l of alum was observed to be small (from 7.5 to 7.2), it may not be necessary to add lime to raise the pH after coagulation to reduce corrosion. Lime systems are typically a nuisance to both operate and maintain. Further investigation of this matter should be conducted during pilot plant testing.

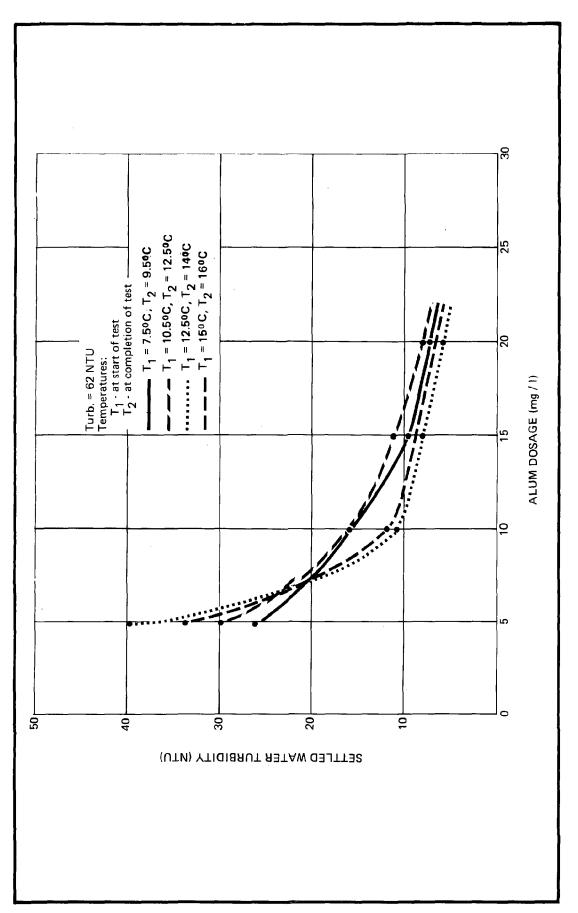


Figure 2-8 Settled Water Turbidity vs Alum Dosage at Various Water Temperatures

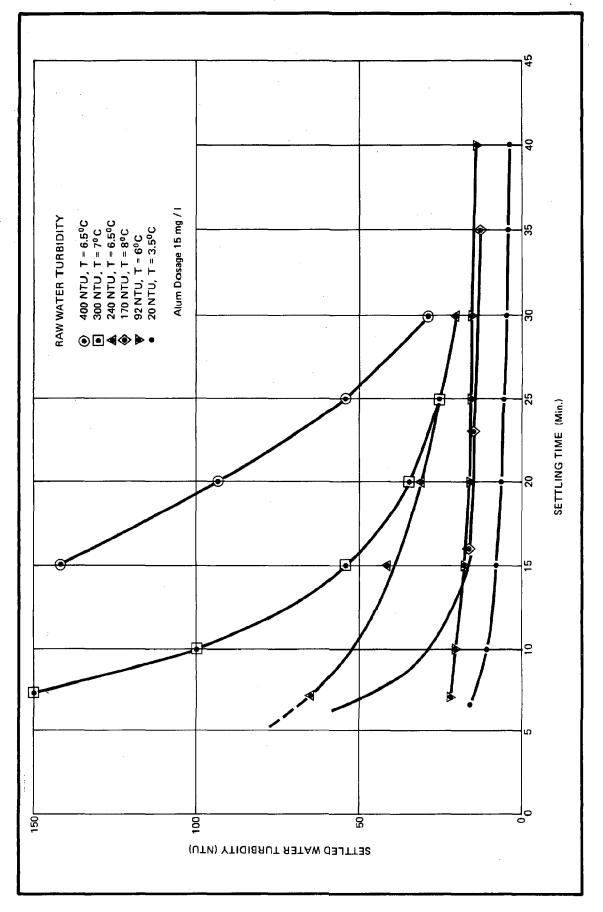
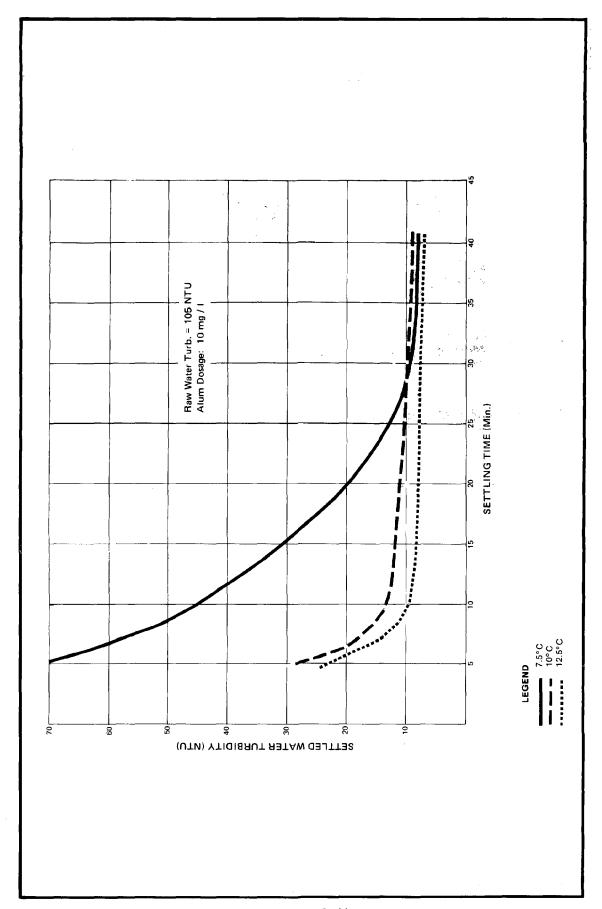


Figure 2-9
Settled Water Turbidity vs
Settling Time at Various
Water Temperatures

Figure 2-10 Settled Water Turbidity vs Temperature and Settling Time



#### TREATMENT REQUIREMENTS

Treatment goals should achieve or exceed the State of Alaska drinking water regulations and the EPA standards as set forth in the National Interim and Secondary Drinking Water Regulations. Table 3-1 lists several of the more common water quality parameters and shows both EPA Maximum Contaminant Level (MCL) requirements and natural levels of these parameters in the Eagle River. The Eagle River water exceeds MCL requirements in only turbidity, color, iron, and manganese.

Table 3-1
WATER QUALITY STANDARDS AND RAW EAGLE RIVER QUALITY

	EPA (MCL) <sup>a</sup>	Raw Eagle River
Physical Factors		
Color (platinum cobalt units)	15	10-70 <sup>b</sup>
Odor (threshold odor No.)	3	-
Turbidity (NTU)	1	5-400
Chemical Factors (mg/l)		
Iron	0.3	4.6
Manganese	0.05	0.1
Chloride	250	0.3-30
Sulfate	250	0.5-38
Nitrate-N	•	0.26
Fluoride	2.4 <sup>C</sup>	0.3
Hardness		34-134
Dissolved Solids	500	41-167
рН	6.5-8.5	6.4-8.1
THM	0.10 <sup>C</sup>	(avg. 7.5)

aMaximum contaminant level.

<sup>&</sup>lt;sup>b</sup>Raw water color is influenced by turbidity; raw water samples were not centrifuged or filtered before color was measured.

<sup>&</sup>lt;sup>C</sup>Maximum for annual average maximum daily air temperature 50 degrees F.

After it was found in Task 1, Well Drilling Program, that the Eagle River Valley does not contain enough groundwater to fulfill the Anchorage area water needs, the Municipality requested that additional testing of Eagle River surface water be conducted for biological quality and for heavy metal and organic chemical content. The results of these analyses (conducted from January to June 1981) are documented in Exhibit B of this report. These results also indicate an excess of color in Eagle River water.

During the eight coldest months when glacial melt ceases, the river is cold (zero to 4 degrees C) with low turbidity (2 to 40 NTU). During the summer, streamflow swells considerably, reflecting glacial melting. In the summer, the river exhibits temperatures ranging from 6 to 8 degrees C and turbidities ranging from 50 to over 400 NTU. The high turbidity caused by glacial flour may seem to present a treatment problem, but highly turbid water actually is more readily treatable. It is cold, low-turbidity water that generally presents the greatest treatment problems.

Experience with Ship Creek water at the Municipal Water Treatment Plant indicates that removal of color and turbidity during periods of low raw water turbidity requires special treatment beyond the addition of 10 to 15 mg/l of alum. The same may be true of Eagle River water. To enhance the coagulation, sedimentation, and filtration processes for effective color and low turbidity removal, lime addition at the headworks or other treatment methods might be required.

In general, Eagle River raw water should be an excellent source of potable water but, prior to final design, it is strongly recommended that a full 1-year pilot plant testing program, using at least a 1-mgd plant, be conducted to establish process design criteria. This testing program should address iron, color, and turbidity removal; chemical dosages required over the full range of raw water parameters; filtration rates and media selection; and effectiveness of the recommended treatment processes.

#### TREATMENT PROCESSES

To satisfy the water treatment requirements most efficiently, the plant will require different operational modes to accommodate summer and winter variations. Figure 3-1 illustrates three possible operational modes: conventional treatment, direct filtration, and in-line filtration. Conventional treatment uses flash-mixing of coagulants, flocculation, sedimentation, and filtration processes. This mode would be applicable during the summer months when the river turbidity is high--over 50 NTU.

Direct filtration uses most of the above processes but would bypass the sedimentation basins. In-line filtration would bypass the flocculation and sedimentation basins but would move the coagulant application point closer to the filters. Both direct and

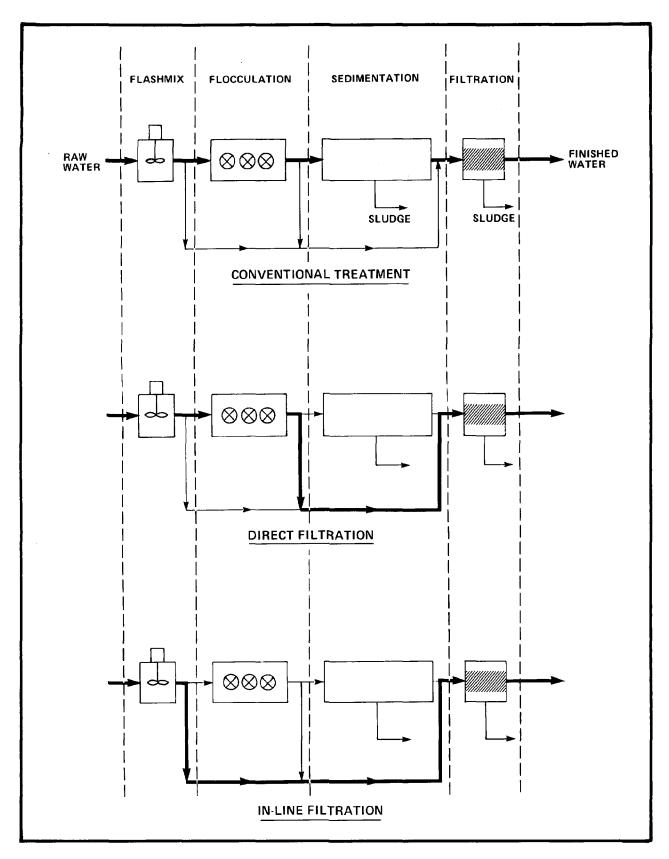


Figure 3-1 Treatment Process Options

in-line filtration should be applicable for Eagle River water treatment during the fall, winter, and spring months when glacial melt is at a minimum and, therefore, raw water turbidity is less than 50 NTU. The feasibility of using direct and in-line filtration should be confirmed by the pilot testing program.

Conventional treatment is compatible with either the direct or in-line process. The transition, seasonally, from one process to the other would be easy. Bypass channels or piping is all that is needed to achieve operational flexibility. As might be expected, operational cost for either direct or in-line filtration will be substantially lower than for conventional treatment because of lower chemical dosages, reduced sludge production, and less equipment maintenance.

#### TREATMENT PLANT

Figure 3-2 shows a typical filtration plant flow schematic, and Figure 3-3 shows a preliminary layout for a 70-million-gallon-a-day plant. The plant could be constructed in increments with basins and filters added when needed with little disruption to continuing operation of existing facilities. From the layout, it can be seen that a 7-acre site will be required.

Although plant site selection is beyond the scope of this task, desirable sites would be those that provide easy access during all weather conditions, minimize pumping requirements through careful site selection at the proper elevation, and eliminate the need for either raw or finished water pumping. Elimination of raw water pumping is more desirable, providing construction cost savings and reduced equipment wear. Finished water pumping can facilitate customer service along the transmission pipeline.

#### Headworks

The headworks contains facilities for application and mixing of chemicals plus a metering device to measure raw water flow into the plant. Chemicals can be mixed by using either an "in-channel rapid mixer" or a metering device such as a Parshall flume,

#### Flocculation

Floc nuclei (aluminum hydroxide) resulting from coagulation join together through numerous contacts and envelop suspended particles in the process. Upon sufficient mixing, the floc grows to a size and density that settle readily.

It is important in both the flash-mixing and flocculation zones that equipment be furnished with variable-speed drives to allow variation in energy inputs. Because optimum mixing requirements vary from season to season, chemicals may be wasted if proper adjustments cannot be made.

Figure 3-2 Typical Plant Flow Schematic

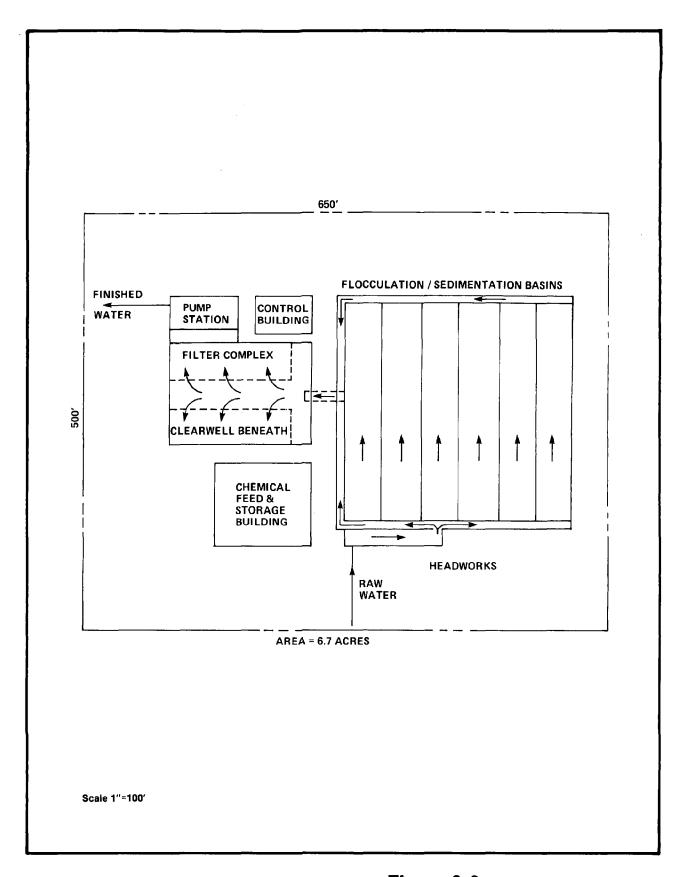


Figure 3-3 Preliminary Plant Layout

#### Sedimentation

Dense floc particles, including suspended solids, settle out in the sedimentation area leaving comparatively clear water containing a minimum of floc. Because of the heavy rock flour load, the sedimentation basins should be equipped with mechanical sludge removal equipment. It is anticipated that between 50 and 150 tons of dry solids sludge will be produced daily during the summer.

#### Filtration System

The settled water from the sedimentation area, containing a small amount of unsettled floc, proceeds to the filters. The filters remove the remaining floc. Granular media filters consist of either two or three layers, each exhibiting a different size and specific The largest grain media having the lowest specific gravity is located at the top of the filter with progressively smaller and heavier sizes toward the bottom. This arrangement permits floc and sediment particles to be removed throughout the entire filter rather than mostly at the surface as typically occurs in single-grain-media filters. The addition of polymer as a filter aid immediately ahead of filtration improves floc removal within a filter, even at higher filtration rates. A nominal filtration rate of 6 gallons per minute per square foot is suggested for an Eagle River filtration plant. Pilot filter testing is needed to (1) verify the design filter rates, both summer and winter; (2) select filtering media specifically for local conditions; and (3) identify which chemicals are needed to aid filtration and in what quantity.

#### Wastewater Disposal

Sludge containing rock flour and sediment from the river is produced in two locations in the plant: the sedimentation basin underflow and the filter backwash water. At a plant flow rate of 70 mgd and a raw water turbidity of 150 NTU, the quantity of sludge produced would equal 55 tons per day of dry solids, which would equal approximately 730 cubic feet per day of solids. Removal of solids from sludge for ultimate disposal is often the most complex problem to be solved in the design of a water treatment plant.

Generally, there are two means for dewatering sludge solids, either by natural means such as evaporation, percolation, and freezing or by mechanical means using such devices as vaccum filters, filter presses, and centrifuges. The cost for mechanical dewatering is usually three to ten times the cost for natural drying.

Natural drying in drying beds or lagoons is the practical choice where climatic conditions permit drying to the degree that the sludge exhibits the characteristics of a solid that can be readily loaded for landfill disposal. Usually two or more beds or lagoons are provided to permit use of one while the other is drying.

More thorough evaluation of the local climatic and geologic conditions is required before a decision can be made regarding sludge disposal.

#### Disinfection

With the addition of disinfection, the water leaving the filters is of potable quality and ready for transmission and distribution to the public. Although chlorine has been the universal disinfectant in public water works, further consideration should be given to the use of other disinfectants for preliminary disinfecting while continued use of chlorine or hypochlorite will likely remain the choice for post disinfection as the water enters the transmission and distribution systems. Further investigation is required prior to selecting disinfectants and their application points within the plant. Trihalomethane formation potential needs to be determined upon selection of Eagle River surface water as supply source.

#### ALTERNATIVE TREATMENT METHODS

Alternative treatment methods were considered, some of which were reported by others in previous studies. These methods include hydroclone separators, screening with microstrainers, and precoat filters. Only precoat filtration is applicable for the Eagle River conditions and could be considered an alternative to granular media filtration. Historically, granular media filtration is the choice for public water supplies, especially installations over 5 mgd. The disadvantage of precoat filtration is the possibility of loss of the precoat from the filtering septum, allowing raw water to short circuit through the filter. Loss of precoat can be caused by hydraulic surges, changing flow rate, power failure, and operator error. Granular media filters are subject to operator error only. Further consideration of the precoat filtration is not considered worthwhile.

#### Chapter 4 COST ESTIMATE

Table 4-1 shows the total project costs for a 70-mgd plant as well as a 23.33-mgd plant, which provides for ultimate plant development in three equal increments.

Table 4-1
ESTIMATED PROJECT COSTS<sup>a</sup>

	Plant	Capacity
	23-1/3 mgd	70 mgd
Capital Construction (Anchorage)	\$10,900,000	\$26,000,000
Contingency, Bonds and Insurance, and Technical, Adm., and Legal Services (Anchorage)	6,459,000	15,400,000
TOTAL Capital Costs <sup>b</sup>	\$17,359,000	\$41,400,000
Annual O&M Labor Chemicals Power Maintenance Materials Miscellaneous	443,000 335,000 193,000 98,000 6,000	895,000 1,006,000 580,000 212,000 17,000
TOTAL Annual O&M Costs	\$ 1,075,000	\$ 2,710,000

<sup>&</sup>lt;sup>a</sup>In January 1981 dollars.

The estimated construction costs and operation and maintenance costs are based on actual experience for plants constructed and operated in the Pacific Northwest and have been adjusted to reflect costs for Alaska. They are also based on the EPA Estimating Water Treatment Costs, Volumes 1 and 2, and on the MAUS, Volume 2. These estimates are considered as order of-magnitude estimates with a -30 to +50 percent reliability range.

Construction costs reflect the use of reinforced concrete construction with all basins and filters being enclosed. The estimates

bLand costs are not included.

include finished water pumping (without standby power) but exclude both raw water and finished water transmission piping and raw water pumping.

Construction costs are in January 1981 dollars using an Engineering News Record Construction Cost Index of 347. Although land costs are not included in the estimates, the site requirements are 7 acres for the plant and 23 acres for the lagoons—a total of 30 acres.

#### Chapter 5 BIBLIOGRAPHY

- U.S. Army Corps of Engineers, Alaska District, in conjunction with the Municipality of Anchorage. Metropolitan Anchorage Urban Study, Volume 2, Water Supply. 1979.
- U.S. Environmental Protection Agency. Estimating Water Treatment Costs, Volume 1, Summary. EPA-600/2-79-162A. Municipal Environmental Research Laboratory, Office of Research and Development. Prepared by Culp/Wesner/Culp Consulting Engineers, Santa Ana, California. August 1979.

Cost Curves Applicable to 200 MGD Treatment Plants. EPA-600/2-79-162B. Municipal Environmental Research Laboratory, Office of Research and Development. Prepared by Culp/Wesner/Culp Consulting Engineers, Santa Ana, California. August 1979.

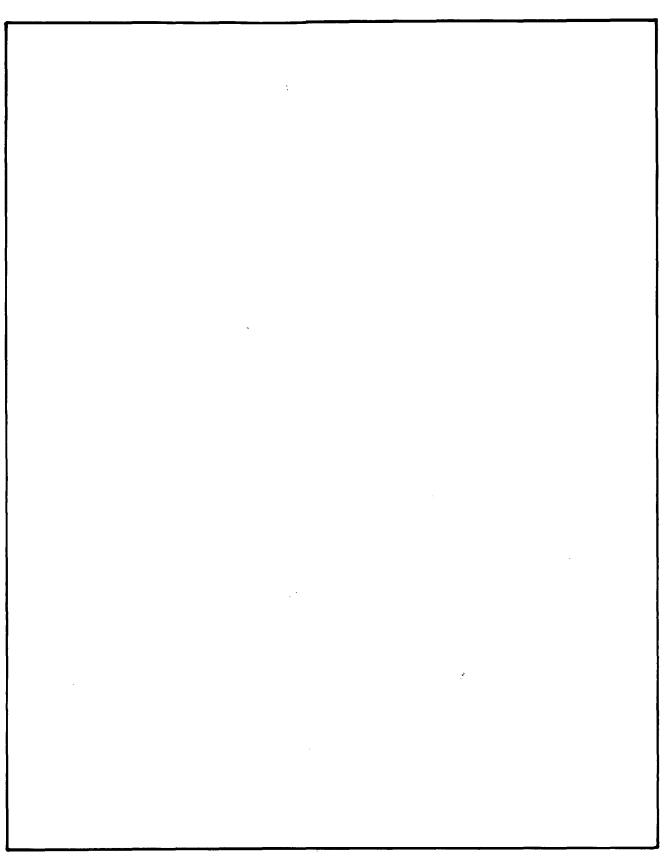


Exhibit A USGS Water Quality Data

UNITED STATES DEPARTMENT OF INTERIOR - SEOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

NITRO- GEN, NITRATE DIS- SOLVED (MG/L AS N)	3.1	;	.27	•23	• 16	.27	.27	• 25	•23	• 32	.16	•14	•29	.11	.07	.27	.38	.27	• 66	• 05
CAR-BUNATE (MG/L AS CO3)	•	0	0	0	0	0	0	o	0	0	0	0	0	0	0	0	0	0	0	0
BICAR- BONATE (MG/L AS HC03)	82	66	S 8	19	53	101	100	93	100	74	3 7	8 7	98	47	67	<b>9</b> *	16	108	46	38
ALKA- LINITY FIELD (MG/L AS CACO3)	67	81	4	52	43	83	82	76	82	61	36	39	7.1	39	52	69	80	68	7.7	31
CARBON DIOXIDE DIS- SOLVED (MG/L AS CO2)	11	;	19	3.4	8 •	16	5.1	5.9	5.1	7.5	11	6.1	4.4	1.9	2.7	3.4	6.2	6.9	7.5	54
PH (UNITS)	11	:	6.7	7.5	7.0	7.0	7.5	7.4	7.5	7.2	6.8	7.1	7.5	7.6	7.6	7.6	7.4	7.4	7.3	4.0
SPE- CIFIC CON- DUCT- ANCE (UMHOS)	174	198	133	146	113	209	211	194	203	152	92	96	190	107	166	192	187	228	207	16
COLOR (PLAT- INUM- COBALT UNITS)	::	:	!	10	ហ	ທ	ហ	ស	ĸ	ហ	ស	rv.	10	ហ	S	ທ	0	0	0	20
SURFACE AREA ( 150 MI) (00049)	192	•	192	192	192	192	192	192	192	192	192	192	192	192	192	192	192	192	192	192
TEMPER- ATURE (DEG C) (00010)	::	1.5	0.6	:	9.5	•	î.	1.0	7.0	10.0	0.6	10.0	•	;	1.5	3.0	ស្	;	9.5	:
H H E	948	1949 1620	1820	;		1000	0060	1200	1300	1600	1430	1800	1		1055	1030		1500	1700	1800
DĂTE	• : :	APR . 10	:-		•	•	12	( (C )		12.	14.			•	•	05.		•	Z.3.	16

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

CHLO- RIDE. DIS- SOLVED (MG/L AS CL)	2.0	:	3.0	ů.	1.2	1,5	1.2	<b>6.4</b>	2.5	2.5	2.5	1.0	80	1.8	<b>.</b>	n.	1.0	2.0	2.5	1.0	1.5
POTAS- SIUM, DIS- SOLVED (MG/L AS K)	;	;	1	:	:	:	:	1	:	1	ļ	:	i	1.0	1.4	4.		5•	•	4	9.
SODIUM+ POTAS- SIUM DIS- SOLVED (MG/L AS NA)	3.2	!	;	2•3	2.7	3.5	8.3	4.1	2.3	0.4	4.7	2.2	3.1	ł	;	i	:	:	:	i	:
PERCENT SODIUM (00932)	;	;	!	;	;	;	;	;	;	1	1	;	:	7	13	Ŋ	7	~	9	ហ	4
SODIUM AD- SORP- TION RATIO	!	i	i	i	;	:	:	ł	:	1	ł	;	:	•-	2.	-	• 1	~		-:	.1
SODIUM. DIS- SOLVED (MG/L AS NA)	1	:	;	•	1	;	:	;	;	;	;	1	:	3.0	3.5	1.9	5.9	3,2	3.6	5.6	σ.
MAGNE- SIUM• DIS- SOLVED (MG/L AS MG)	4.	:	1	3.4	3.5	5.6	S.5	5.1	5.1	6.1	4.3	2.6	3.0	5.1	1.5	5.1	4.8	6.3	8.4	5.7	2.9
CALCIUM DIS- SOLVED (MG/L AS CA)	27	:	;	50	21	17	33	33	30	32	23	14	15	28	17	54	28	56	32	31	13
HARD- NESS, NONCAR- BONATE (MG/L CACO3)	18	-	:	16	12	10	25	54	20	23	14	10	11	20	10	56	21	11	25	54	13
HARD- NESS (MG/L AS CACO3)	96	ŀ	:	99	19	53	105	106	96	105	75	46	20	16	64	6	06	16	114	101	77
HA NE (ME (A) (A)	OCT , 1948	19		200 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	•	200	21	12	16.	E 0	12.	14.	22		04		000	10	•		Joe 16

UNITED STATES DEPARTMENT OF INTERIOM - GFOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

_
⋖
-
•
_
0
>
_
- 1
_
AL
9
_
$\sim$
_
$\sim$
ч.
TER
_
_
A
_

ELEV. OF LAND SURFACE DATUM (FT. ABBOVE	(72000)	250.00	:	:	250.00	0000	00.002	250.00	250.00	250.00	250.00	250.00	250.00	250,00	250.00	250.00	250.00	250.00	250.00	250.00	250.00	250.00	250.00
IRON (UG/L AS FE)	(71885)	;	:	i	i	76	0	30	40	04	140	140	30	130	240	0	0	40	20	0	0	20	100
MANGA- NESE (UG/L AS MN)	(71883)	;	:	1	;		;	•	:	;	:	;	:	;	;	10	0	0	0	0	0	10	;
NITRO-GEN• NITRATE DIS- SOLVED (MG/L AS NO3)	(71851)	-		;	2.		0 • 1	.70	1.2	1.2	1.1	1.0	1.4	.70	•60	1.3	.50	•30	1.2	1.7	1.2	5.9	.20
SOLIDS. DIS- SOLVED (TONS PER AC-FT)	(70303)	41.		;	~~		11.	60.	.18	.18	.16	.17	.13	90.	60.	.15	60.	.13	.15	.16	.19	.16	.07
SOLIDS. SUM OF CONSTI- TUENTS. DIS- SOLVED	(70301)	501	) I	;	61		86	89	142	129	112	128	4	58	9	110	9	96	111	114	137	120	53
SOLIDS, RESIDUE AT 180 DEG. C DIS- SOLVED (MG/L)	(70300)	i	•	;	;		1	;	129	130	118	;	;	;	i	i	1	1	!	i	;	!	:
SILICA, DIS= SOLVED (MG/L AS SIO2)	(00955)	0,6	; ;	!	6.4	. i	•	3.0	4.9	7.1	6.3	9.9	5.2	3.4	4.1	5.0	2.6	3.2	7.2	0.6	8 • 9	7.7	2.3
FLUO- RIDE. DIS- SOLVED (MG/L AS F)	(05600)		: :	;	1		E.	;	•1	0.	•1	.1	• 1	0.	i	0,	0.	•	0.		0.		0.
SULFATE DIS- SOLVED (MG/L AS SO4)	(00945)	976	u	546 54	<u> </u>	951	<b>*</b>	13	36	54	19	56	19	12	15	956 22	15	28	54	17	27	92	13
C 4 A A	1	-	: :	- :	JUN 245	-	NUC	:	:	12.	¥ 9 7	08.	12.	14.	:	-:	2040.	020	050	1000	23.	7AY	16

5

UNITED STATES DEPARTMENT OF INTERIOR - SFOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

BICAR- BONATE (MG/L AS HCO3) (00440)	32	i	104	;	114	90	:	68	04	1	•	•	} }	1	İ	# # # 1	: :	:	•	:	:	•	:   		;	; ;	\$   <b>8</b>	!
ALKA- LINITY FIELD (MG/L AS CACO3)	26	:	85	;	0 I	4 6	:	92.			:	<b>9</b> (	; ;	1	;	1 1	:	1	;	•	!	• •	1 1		:	1 1	<b>9</b> (	l B
CARBON DIOXIDE DIS- SOLVED (MG/L AS CO2)	91	•	5.6	:	0 • 1 1 • 8	3.6	;	2.2	9:1		;		1 1	1	!	: :	1	1	;	1	•	•	•	1	;		1	! •
PH (UNITS) (00400)	6.5	:	7.8	:	7.5	7.6	•	7.7	9.2		: :	• •	; ;	;	.;	: 1	1	!	i	!	!	:	•	1	;	;	• 1	) 
SPE- CIFIC CON- DUCT- ANCE (UMHOS)	76		243	222	286 286	197	151	151	400	1 4	87	0 (	ა ტ ი	95	95	10 C	9 A	83	83	S.	11	-;		~ ! - i	7	± ;	77	1 /
COLOR (PLAT— INUM— COBALT UNITS)	30	:	'n	•	ហ៖	ហេវេ	•	R	ហ		1	<b>!</b>	1 1	;	1	1 1	1	1	1	!	;	•	!	;	!	•	:	<u>!</u>
STREAM- FLOW. INSTAN- TANEOUS (CFS)	i	1160	:	95	0 U 4 4	155 193	747	742	1650	,	<b>:</b> :	1	<b>!                                    </b>	1	•	;	<b>:</b>	ł	;	i	:	:	!	1	•	:	;	!
CHARGE.  IN CUBIC FEET PER SECOND (00060)	ł	;	:	1	11	;;	:		1 1	1 000	2140	1500	1450	1580	1470	1410	1860	2180	2130	2410	2580	1790	2980	2830	2310	0912	0052	0102
SURFACE AREA (SO MI) (00049)	192	:	:	:	::	192	;	:	192	1	: ;	•	<b>!</b>	;		•		1	;	;	1	1	:	;	•	;	1	1
TEMPER- ATURE (05G C)	9.0	0.9	S.	0.	00	4 6 0 8				•	7.0	•	0 0		•	œ -		2	:	2	•	•	ė «	•	٠	•	•	•
T 1ME	1958 1145	1300	1200	1200	1130	1100	1045	1115	1340	1400	1730	74	1730	80	74	7 7	. E	73	80	80	73	2.0	2 6	80	80	. 3	e c	r r
DATE	• •	13.	500	9.0			•			_	30.	:	0 C		0 A	•			13	14	15.			•	22.		٠	5.00

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

CHLO- RIDE, DIS- SOLVED (MG/L AS CL)	3.0	:	1.4	:	=======================================	1.4	•	44	: :	:	:	!	: :	•	;	1	! !	1	;	•	1 1	;	1	:	:	:	:
POTAS- SIUM. DIS- SOLVED (MG/L AS.K)	1.2	:	e.	:	ω <u>;</u>	ທຸຕຸ	1		: ;	•	<b>!</b>	!	: 1	•	;	:	: :	;	•	1	<b>:</b> 1		:	!	1	•	;
PERCENT SOBLUM (00932)	ហ	;	Ŋ	:	ν i	7	•	100 1	- ;	:	:	•	: :	1	:	;	: :	;	;	:	; ;	1	;	1	•	1	i i
SODIUM AD- SORP- TION RATIO	• 1	;		ł	1:1	- 2	;		: :	1	;	!	! !	:	;	;	: ;	;	;	:		: :	!	;	1	;	1
SODIUM, DIS- SOLVED (MG/L AS NA)	<b>6</b> 0	ł	2.7	:	3.1	3.6 8.8		2.7	1	:	<b>;</b>	;	1 1	: :	1	!	! !	1	1	!	6 I	<b>:</b> :	<b>:</b>	;	!	!	:
MAGNE- SIUM, DIS- SOLVED (MG/L AS MG)	5.4	;	4.	;	5.2	3.4	;	(M)	• 1	•	•	•	! ;	<b>:</b>	;	;	<b>!                                    </b>	;	!	1	: :	: ;	:	•	!	;	}
CALCIUM DIS- SOLVED (MG/L AS CA) (00915)	6.6	:	36	;	45	32	;	19		:	<b>!</b>	!	• (	<b>;</b> ;	1	;	1 1	;	1	!		1 1	1 1	i	;	;	1
HARD- NESS. NONCAR- BONATE (MG/L CACO3)	œ	!	23	•	91	17			- 1	!	ļ	;	! !	: :	1	:	: ;	:	:	!	1 ( 1 (	i ;	: :	:	;	:	;
HARD- NESS (MG/L AS CACO3)	9. 4	:	108	:	134	56 40 90	. !	1 6	; ;	!	•	;		1 1	1	1	1 1	;	•	1	1		<b>:</b> :	. ;	;	;	;
NITRO- GEX. NITRATE DIS- SOLVED (MG/L AS N)	• 05	i	.18	:	•25	.23		70.	51	1	•	;	* 1	1	;	;	! ;	!	!	!	•		: :	;	1	!	•
CAR- BONATE (MG/L AS CO3)	958 0	996	0	;	0	<b>c</b> 0	• •	00		1	:	;	• (	<b>:</b>	;	1	; ;	ļ	•	•	! !	1	: :	:	;	;	:
DATE	AUG . 1	13.	26.	•	• •	₩ 7 4 0	NON W		29.	59	30 JUL	01	0.4.0	90	0.8	09.		12	13	14	15.	200	200	22	23.	24	25

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY 15277100 - EAGLE P AT EAGLE RIVER AK

SED. SUSP. FALC DIAM. # FINER THAN (70341)	;	69	;	:	ł	;	;		;	;	:	•	:	:	;	:	:	•		}	;	;	;	į	1	!	İ	i	İ	:	;	;
SED. SUSP. FALL DIAM. % FINER THAN (70340)	;	62	1	:	:	:	1	•	1	;	:	:	:	•	•	;	•	:	• •	; ;		:	;	:	;	;	:	:	•	•	•	<b>!</b>
SED. SUSP. FALL DIAM. & FINER. THAN (70339)	;	52	;	:	;	;	:	:	1	:	;	!	:	;	;	!	!	;	•	}	: :	;	;	;	;	;	!	:	;	1	:	;
SED. SUSP. FALL DIAM. % FINER THAN (70338)	;	04	i	:	:	:	;	:	;	;	1	:	:	:	:	i	:	:	:		:	1	;	:	i	i	:	;	;	!	!	ļ
SED. SUSP. FALL DIAM. & FINER THAN (70337)	;	30	!	1	;	;	:	!	!	!	;	1	:	•	;	!	1	1	!	• !	! !		!	:	ŀ	!	:	!	!	1	1	1
SOLIDS, DIS- SOLVED (TONS PER AC-FT)	90•	:	.17	:	.23	:	•16	•17	ţ	.11	• 0 7	•	;	:	;	:	:	:	!		: 1	1	;	•	;	:	;	;	;	:	:	!
SOLIDS. DIS- SOLVED (70NS PER DAY)	ŀ	;	1	;	24.3	:	49.0	63,6	:	160	4	;	:	:	;	1	;	:	:	•	; ;	:	;	;	;	!	3	:	:	;	1	!
SOLIDS, SUM OF CONSTI- TUENTS, DIS- SOLVED (MG/L)	<b>4</b> Ծ	:	127	:	167	!	117	122	:	80	54	!	:	:	;	!	:	1	•		:	:	•	;	;	;	1	1	;	!	;	ŀ
SILICA. DIS- SOLVED (MG/L AS SIO2) (00955)	2.0	1	5.9	;	7.2	;	4.4	4.5	1	3.5	3.2	:	1	1	;	1	:	;	<b>!</b>	• •	; ;	1	;	;	;	1	•	!	1	;	1	•
FLUO- RIDE+ DIS+ SOLVED (MG/L AS F)	0.	;	•1	:	0.	:	e,	4.	!	۰.	•	:	:	•	1	;	!	:	•	<b>:</b>	: :		;	;	;	:	;	!	1	;	;	1
SULFATE D1S- SOLVED (MG/L AS SO4)	1958	9961	54	:	1967 31	:	92	52	:	16	15	;	;	:	ł	1	!	!	1 1	1 1		:	:	;	ŀ	:	!	;	!	!	;	!
DATE	•	. :	200 200 200 200 200 200 200 200 200 20	•	20	20	04	12	050	05	29	29.	29.	30. JUL	01	04	n	0.6		,				14	15	19	20	21	22	23	24	25

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

Α¥	
KIVER	
EAGLE	
RATE	
EAGLE	
15277100 -	

	SEDI- MENT, DIS- CHARGE, SUS- PENDED	(7/04Y) (80155)	;	1	966	;	3.7	•	•	27	7.7	353	:	:	949	1380	3080	919	565	360	905	23%	379	964	945	857	1540	1000	0000	3000	1770	818	1810	1980
	SEDI. MENT. SUS. PENDED	(MG/L) (80154)	ţ		318	•	16		£.	05	<b>93</b>	176	•	:	145	252	532	152	132	92	212	ט ע ר	n m	192	160	149	236	152	717	0021	0 00	139	292	292
	ELEV. OF LAND SURFACE DATUM (FT.		250.00	) ) !	;	1	;	1	;	250.00	;	;	;	250,00	1	!	:	;	•	•	;	;	1	;	i	:	;	;	;	1 1	:	;	1	;
	IRON (UG/L	AS FE) (71885)	00	ì	:	04	:	320	!	1300	400	1	1150	2300	1	!	:	:	:	!	!		1 1	i	;	:	ľ	ł	1	1 1	1	ł	1	1
	MANGA- NESE (UG/L	AS MN) (71883)	~		:	!	i	:	i	:	:	!	:	:	i	!	ł	1	1	•	1	1		•	•	!	!	1		•	; ;	1	!	;
ITY DATA	NITRO- GEN. NITRATE DIS- SOLVED (MG/L	AS NO3)	00.	1	:	•80	•	1.1	:	1.0	1.1	:	06.		; <b>;</b>	:	;	;	1	ŀ	!	•	: :	;	1	1	î	i t	ł	<b>1</b> 1	1 1	1	1	!
WATER QUALITY DATA	<b>8</b> €	1.00 MM (70346)	:		100	!	!	:	:	!	:	100		; ;	:	:	:	!	;	:	!	!	! !		;	•	:	:	!	•	! !	•	1	;
3	SED. SUSP. FINER THAN	.500 MM (70345)	i		66	:	;	;	•	!	•	0	: ;	i	100	:	;	1	;	i	1	!	1 1	;	;	1	1	;	!	f	1 1	+	;	;
	SED. SUSP. FALL DIAM. FINER	.250 MM (70344)	;	ı İ	76	;	!	1	:	;	•	ď		: :	91	;	;	;	1	1	1	;	1 1		;	•	:	1	:	i i	• •	1	1	1
	SEO. SUSP. PALL FINER. THAN	.125 MM (70343)	:		48	;	ł	;	<b>!</b> .	;	•	7.7	: :	i	76	1	:	į	1	;	1	,	: :	;	;	;	•	!	;	\$   1	: :	1	;	;
	SED. SUSP. FILL TINER	.062 MM (70342)	958	996	75	;	1967	:	:	•	:	ď	2 1	i	69	•	•	:	;	;	;	;	: :	;	;	1	;	† 1	;	:	: :	: :	;	;
		DATE	<b>~</b> ,		13	26 10V	• ~	•	20. 18 Y	04	12	2 Z	100	0	29.	62	30	01.	04.	05	06				12.	13	14	15	19.	20		700	24	25

UNITED STATES DEPARTMENT OF INTERIOR - GFOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

BICAR- BONATE (MG/L AS HC03)	:	;	;	;	: :	;			1 1	:	•	•	;	;	:	:	:	:	:	;	ď	<b>:</b>	: :		•	80	:		25	30	;	;	:
ALKA- LINITY FIELD (MG/L AS CACO3)	!	:	;	•	•	:	(		1	;	;	;	ì	;	:	:	:	:	•	!	9.	) (	1 1		;	ď	: 1		£4	52	1	:	;
CARBON DIOXIDE DIS- SULVED (MG/L AS CO2)	:	;	:	•	•	;	1	;	1 1	•	;	;	;	ŀ	:	:	;	:	;	:	4		1 1	i	•	0.4	1		2.1	1.5	;	:	ţ
PH (UNITS)	ì	;	,		1	1	!	1	}		:	:	;	;	:	:	1	:	1	:		7 .	1 1	1	!	7.4	: :		7.6	7.5	ļ	:	1
SPE- CIFIC CON- DUCT- ANCE (UMHOS)	12	• Q	-	- a	77	14	1.	- 0	0 0	G (C	2.5		69	69	77	90	7.1	7.1	40	87	۲	101	101	7	;	100	) † 		113	74	175	225	233
COLOR (PLAT- INUM- COBALT UNITS)	:	1	. !			;	į		1 1		•	;	;	:	•	•	!	!	!	1	,	01		1	:	c	) <u> </u>		ហ	S	;	;	1
FLOW. INSTAN- TANEOUS (CFS)	•	i 1	; ;	}	1 1	1			•	: :	: :		ļ	;	1	:	ļ	•	3110	ł	000	0.00	000	11261	777	0	, <b>0</b>	ì	1520	1650	194	100	<b>ያ</b>
CHARGE.  IN  CUBIC FEET PER SECOND	0480	1930	000	1860	1900	2000	2770	- 6	0000	2170	2410	2370	2910	2970	2280	1950	3150	3020	!	1360	1			i	•	i	;		:	ł	;	1	1
SURFACE AREA (SQ MI) (00049)	,	<b>:</b> !	1 1	1 1	1	1		1	!	1		;	;	;	:	1	!	!	•	;		1	1	<b>!</b>	!	1			192	192	1	1	1
TEMPER- ATURE (DEG C) (On10)			•			ທ ໝ		•	•	•	à		7.0					•	•	•	. !	1 U	•		2.0	0.4	4		8.0	7.0	4.0	0•	0•
3 1 1	~	) r	. a	2	2	1830	2		ָ ק	7	2	ď	1900	0	0	0	m	3	0	80		i c		2		0	1100	•	1500	1300	1400		1100
DATE	_		•	•	30			•	•	96					60	11	14	15	17	22.		٠	•	00T	:		90	•	03	13	03	27	MAR . 10

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY 15277100 - EAGLE P AT EAGLE RIVER AK

																				٠											
CHLO- RIDE, DIS- SOLVED (MG/L AS CL)	:	1	! !	1	:	!	1	1	:	:	!	; †	3 ! 6 1	; ! ; i	; ;	1 1	ł	:	;		;	<u> </u>	:	1.8	:	•	o.	œ,	:	:	;
POTAS- SIUM, DIS- SOLVED (MG/L AS K) (00935)	ł	1	• •	<b>:</b>	;	1	•	;	:	;	1	! !	•	• 1		1	:	1	:	1.4	;	1	1	4.	-	(		9.	1	;	;
PERCENT SODIUM (00932)	:	1	• !	! !	;	;	;	!	!	!	!	!	9 1		. !	!	1	i *	1	vo	!	!	;	7	į	r	•	ις	!	;	!
SUBTUM AD- SORP- TION RATIO (00931)	i	1	•	1	:	1	1	ł	ŀ	ł	1	:	:	•	:	}	!	!	:	-	1	:	i	2.	:	•	<b>.</b>	• 1	1	:	:
SODIUM, DIS- SOLVED (MG/L AS NA)	:	•		: :	ì	;	:	1	;	1	;	!	ļ	!	!	!	1	!	;	1.6	;	;	;	8,6	1	1	1.1	<b>o.</b>	;	•	1
MAGNE- SIUM, DIS- SOLVED (MG/L AS MG)	;	:	1 (		;	;	;	;	!	1	}	;	1	1	!	:	!	!	;	3.5	1	;	:	χ, γ,	1		5.6	1.7	;	;	1
CALCIUM OIS- SOLVED (MG/L AS CA)	!	1	!	: :	ł	:	:	1	}	;	1	ł	!	1	!		ţ	;	;	17	:	:	!	80	1		9	11	1	ł	ł
HARD- NESS. NONCAR- BONATE (MG/L CACO3)	;	:	[ (	<b>:</b> ;	1	:	ŧ	1	1	!	ļ	;	:	:	:	:	!	:	;	10	;	ł	:	60	1	•	_	6	;	1	:
HARD- NESS (MG/L AS CACO3)	1	1	1	1 1	;	;	;	:	!	!	ŀ	;	;	!	;	!	•	!	1	58	•	1	;	120			<b>1</b> 0	34	;	;	1
NITRO- GEN. NITRATE DIS- SOLVED (MG/L AS N)	;	:	• •	<b>!</b> ;	1	;	:	1	•	!	!	•	:	•	•	!	•	1	•	.23	;	1	;	8.	: !	•	• 05	• 05	:	1	ŧ
CAR- BONATE (MG/L AS CO3)	1961	:	:	<b>:</b> ;	ţ	;	;	;	1	!	!	;	1	r	1	:	;	1	:	c	;	:	8701		1		c	O	ł	;	1 6951
DATE	.:	27	# # # # # # # # # # # # # # # # # # #		31.	01.	0.2	03	04	05	06.	0.20	280	•••60		14	15.	17	22. GFP	19.	19	21 OCT	0.4	1 6 1 70	06.	JUL	03	130	03	_	

UNITED STATES DEPARTMENT OF INTERIOR - GFOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVEH AK

SED. SUSP. FALL DIAM. & FINER THAN .016 MM	111	1111	1111	!!!!!	11131	68 1	11 9 6	5 1 1
SED. SUSP. FALL DIAM. % FINER THAN (70339)	1 1	!!!!	1111	11111	11141	61 1 61		3 1 1 1
SED. SUSP. FALL DIAM. % FINER THAN (70338)	111	1 1 1 1	1111	11111	11171	2231	11 4 4	† † † †
SED. SUSP. FALL DIAM. % FINER THAN (70337)	111	! ! ! !	::::	11111	1321	1 4 4 1 ~ 10	31 12	
SOLIDS, DIS- SOLVED (TONS PER AC-FT)	; ; ;		1111	11111	11111	c       ;	6 0	
SOLIDS. 01S- SOLVED (TONS PER DAY) (70302)	111		1111	11111		98 99	792	
SOLIDG. SUM OF CONSTI- TUENST. DIS- SOLVED (MG/L)	1 1	: : : :	!!!!	11111		£11 + 3	134 65	:
IRON, TOTAL RECOV- ERABLE (UG/L AS FE)	1 1 1		1111	!!!!!	11111	111 1	1600	
SILICA. DIS- SOLVED (MG/L AS SIO2)	11	1111		11111		F 1 1 5		
FLU0- RIDE: DIS- SOLVED (MG/L AS F)	111		::::	!!!!!	:::::	0       -		:
SULFATE 015- SOLVEN (M6/L AS SO4) (00945)	1967	1111	1111	11111	1,1111	1969	13	696
DATE	Jul. • 19 26	2000 2000 2000 2000	AUG 000000000000000000000000000000000000	000000000000000000000000000000000000000	111 14 17 17 17 SEP	19 21 0CT 04	06 JUL 03 8UG	007 03 NOV 27 MAR 1 19

UNITED STATES DEPARTMENT OF INTERIOR - GFULUGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AR

۹	
ΛŢ	
à	
₹	
Ξ	
Ţ	
₹	
õ	
x	
ш	
-	
∢ 3	

្រុះឃុំ ដែ្កិ៍			;	1~	N N
SEDI- MENT. DIS. CHARGE. SUS. PENDED (1/DAY)	1630 1040 766 864 867 853	5800 1010 11160 1380 2200	1446 985 4450 2890 4150 632	53	550 615 4.1
SEOI- MENI, SUS- PENDED (MG/L)	243 200 150 172 169 158	775 173 179 189 235 288 337	- M - M - M - M - M - M - M - M - M - M	399 44 + 44 100	134 138 8
ELEV. OF LAND SUMFACE DATUM (FT. ABGVE NGVD)	111111	1111111	111111 11	1 1 11	250.00
180N (UG/L AS FE) (71885)	111111	11111111	1,1111111111111111111111111111111111111	1 1 0 11	1100
NITRO- GEM. NITRATE DIS- SOLVED (MG/L AS NO3)	111111	1111111	1111111 01	1 0 0 1	. 20
SED. SUSP. FALL DIAM. FINER THAN 1.00 MM	111111	11111111		100	1 1 1 1
SED. SUSP. FALL DIAM. R FINFR THAN 500 MM (70345)	111111	11111111	111101 10	6 1 11	100
SED. SUSP. FALL DIAM. % FINER THAN .250 MM	111111	11111111	111191 10	6 1 11	6 6 1 1
SED. SUSP. FALL DIAM. % FINFR THAN .125 MM	111111	11111111	111161 16	26	8 6 8
SED. SUSP. FALL. BIAM. # FINER THAN! .062 MM	111111	1111111	31 14111	S	88 80 1 1
SED. SUSP. FALL DIAM. FINEX. 71AN.	7967	;;;;;;;;		768	7 7 1 1
0 A T E	200 200 200 300 300 300 300 300 300 300	0010 000 000 000 000 000 000	0 1 4 0 1 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0	_	JUJE 03 13 05 NOV

UNITED STATES DEPARTMENT OF INTERIOR - CEULOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

BICAR- BONATE (MG/L AS HC03)	104	ł	1	•	;	9 +	1	109	1 1	100	72	53	84	18	102	91	;
ALKA- LINITY FIELD (MG/L AS CACO3)	85	:	;	!	;	8 E	;	68	1;	8	26	£ <del>1</del>	39	99	84	75	1
CARBON DIOXIDE DIS- SOLVED (MG/L AS CO2)	2.1	1	;	;	;	1.5	;	2.2	::	1.3	10.	1.3	r i	1.3	2.1	2.3	;
РН (2017/15)	7.9	;	1	•	;	7.7	1	6.1	::	8	8.1	7.8	0   0	01	4.7	7.8	1
SPE- CIFIC CON- DUCT- ANCE (UMHOS)	233	217	146	81	109	113	509	233	172 172	212	157 157	121 121	112	186 186	228	195 195	133
COLOR (PLAT- INUM- COBALT UNITS)	0	1	;	i	;	0	1	0	11	! 0	10	w į	ហៈរ	<u>ا</u> ۱	¦	r.	1
STREAM STAGE (FT ABOVE DATUM)	;	!	1	ł	1	7.34	;	!	::	!!	: :	11	! !	11	;	! !	1
STREAM- FLOW. INSTAN- TANEOUS (CFS)	53	106	266	1660	299	0762	121	06	78 78	279	670 670	866 866	784 793	168 168	4	120 120	715
TEMPER- ATURE (066 C)	0.	1.0	7.0	6.0	7.0	4.0	0	0.	4 4 մ.ս.	8 0.8	8 8 0 •	8.0	6.0	ភ.ភ.	0•	44	6.5
Ξ Σ L	1969 1200	1230	1245	1130	1530	1430 1515	1500	1200	1000	1030	1445	1400	1030	1115	1230	1030 1300	1330
DATE	MAR + 19	20 X	M&Y 27	JUL 15	20.00	97. 97.	DEC 16	. :	62	AAY 21 21	16. 16.	28 28	200 200 200 200 200 200 200 200 200 200	::	10	19.	21

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

MAGNE- SIUM• DIS- SOLVED (MG/L AS MG)	6.1	:	ľ	•	!	3.2	: :	5.0	:	;	1.5	; ;	3.6	2.8	;	2.6	!	4.5	!	:	70.5	<b>!</b>	:
CALCIUM DIS- SOLVED (MG/L AS CA)	32	;	;	;	1	15	: :	37	1	:	35	;	24	18	;	17	;	59	:	;	31	:	:
HARD- NESS* NONCAR- BONATE (MG/L CACO3)	21	;	;	;	;	13	: :	52	i	•	20	: 1	17	12	;	14	1	56	;	58	23	1	;
HAMD- NESS (MG/L AS CACO3)	106	!	•	ł	:	12 T	: :	114	;	;	101	. !	92	52	1	53	1	92	;	113	86	;	i
PHOS- PHATE. ORTHO. DIS- SOLVED (MG/L AS PO4)	;	!	i	;	;	: :	: :	;	;	!	100	1	:	1	;	!	;	;	:	;	;	!	;
PHOS- PHATE, TOTAL (MG/L AS PO4)	!	;	;	i	;	1 1	1	;	;	1	1 1	; ;	<b>;</b>	;	;	;		!	•	;	1	}	;
NITRO- GEN, NITRATE DIS- SOLVED (MG/L AS N)	.36	ł	;	:	!	.18	: ;	.32	;	!		: 1	•23	.16	:	.07	:	.27	;	;	• 36	;	:
NITRO- GFN• AMMONIA DIS- SOLVED (MG/L AS N)	i	ľ	!	i	1	: :	. 1	ł	;	1	1000	,	:	:	!	!	ľ	;	:	;	i	1	:
NITRO- GEN• ORGANIC TOTAL (MG/L AS N)	;	;	:	1	;	; ;	: :	;	ł	1		. ;	1	;	1	1	:	1	;	;	;	ì	!
CAR- BONATE (MS/L AS CO3)	<b>C</b>	ł	!	;	;	c		c c	;	•	0		0	c	1	c	;	c		c	;	;	ï
B DATE A	MAR , 1969 26	200 200 200 200 200 200 200 200 200 20	27	15 15	20.0	07	0EC 16	MAR , 1970	A P.R.			JUN	16	22	72 AUG	7 B	78 OCT	15	15 MAR : 1971	:	19	19••• Jak	21

UNITED STATES DEPARTMENT OF INTERIOR - GFOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

	MANGA- NESE, DIS- SOLVED (UG/L AS MN)	•	!	:	:	;	;	•	;	:	;	:	;	;	!	i	•	:	;	:	100	:	i	110	•	;
	IRON• DIS- SOLVED (UG/L AS FE) (01046)	i	;	;	:	!	:	:	;	;	•	:	1	1	;	:	;	1	:	;	40	;	:	100	;	:
	SILICA, DIS- SOLVED (MG/L AS SI02) (00955)	4.0	;	:	;	;	3,3	;	;	3.5	;	;	;	4.3	;	3.1	3•3	!	2 <b>.</b> 8	;	4•1	;	1	4.5	;	;
	FLUO- RIDE: DIS- SOLVED (MG/L AS F)	•1	1	:	;	;	0.	:	1	0.	:	1	;		1	-:			0	1	0.	1	!	7.	1	1
¥⊥	SULFATE DIS- SOLVED (MG/L AS 504) (00945)	92	:	;	;	!	18	!	:	28	;	:	1	23	;	20	16	;	15	;	21	;	;	25	;	;
WATER QUALITY DATA	CHLQ- RIDE. DIS- SOLVED (MG/L AS CL)	3.2	;	;	;	ţ	۲,	Ì	ţ	1.4	1	;	;	4.	;	7.	۳,	;	1,5	;	1.5	;	;	1.8	1	1
WATER C	POTAS- SIUM. DIS- SOLVED (MG/L AS K)	1.4	•	;	!	;	2.2	1	!	ហ្	1	;	!	ស្	;	4	4.	!	4.	!	4.	!	¦	۲.	;	ł
	PERCENT SODIUM SODIUM	^	;	i	I	:	•	!	ł	9	i	1	;	7	ł	-	vo	:	c	;	c	ï	;	7	1	1
	SONTUM AD- SORP- TION RATIO		;	;	}	;		;	i	<b>.</b>	1	;	;	٥.	;	7.		!	-	;		:	;	٠.	:	1
	SONTUM,	1969 3.5	1	;	;	;	1.7	1	1970	3.6	;	;	;	3.6	;	2.5	1.8	;	~ ~	;	5.9		;	С Г	;	;
	DATE	MAR + 19	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	27	15	20.05	07	26	: .	•	29	29	21	21	16.	•	30r 22•••	25°	96.	28.	15	15.00	. :	MAY 19	19	21

SCHLINGS - STATES DEARWITERIOR - GROLOGICAL SURVEY SIGN - STATES DEARWITERIOR - GROLOGICAL SURVEY SIGN - STATES DEARWITERIOR - GROLOGICAL SURVEY SIGN - STATES DEARWITERIOR - GROLOGICAL SURVEY SIGN - STATES DEARWITERIOR - GROLOGICAL SURVEY SIGN - STATES DEARWITERIOR - GROLOGICAL SURVEY SIGN - STATES DEARWITERIOR - STATES DEARWITERIOR - STATES DEARWITERIOR - STATES DEARWITERIOR - STATES DEARWITERIOR - STATES DEARWITERIOR - STATES DEARWITERIOR - STATES DEARWITERIOR - STATES DEARWITERIOR - STATES DEARWITERIOR - GROLOGICAL SURVEY SIGN - STATES DEARWITERIOR - STATES DEARW	PH DISTRICT O		SED. SUSP. FALL DIAM. % FINER THAN 125 MM	;	:	83	85	16	68	1	!	:	: :	ł	:	1 1	}	90	1 6	) }		:	1	16	89
STATES STATES DEPARTIFENT OF INTEHTOR — GFOLOGICAL  STATES STATES DEPARTIFENT OF INTEHTOR — GFOLOGICAL — GFOL	٥		SED. SUSP. FALL DIAM. FINER THAN 062 MM	!	:	73	82	68	81	}	:	;	11	;	•	; ;	}	73	1 6	0	1 1	•	;	1 80	11
SULTED STATES DEPARTMENT OF INTERIOR - 15277100 - EAGLE HAVER GOLDS HAVER GUALITY DATA WATER GUALITY DATA WATER GUALITY DATA SCHOOL SHIPS HAVE SCHOOL SHIPS					;	65	;	:	1 1	}	•	;	11	;	:	; ;	}	11	;	:	1 1	<b>;</b>	1	::	:
SCLINS, SOLIDS, SOLIDS, SCD, SED, SED, SCH OF AT MATER GUALITY OF STATES DEPARTMENT OF SCOLIDS, SOLIDS, SUSP			SED. SUSP. FALL DIAM. % FINER THAN .016 MM	i	:	46	99	;	9	•	1	:	!!	:	1	; ;	1	11	;	:	•	<b>!</b>	;	1 0	!
SCLINS, SOLIDS, SOLIDS, SCD, SED, SED, SCH OF AT MATER GUALITY OF STATES DEPARTMENT OF SCOLIDS, SOLIDS, SUSP	NTERIOR - GLE RIVER	A	01-	1	1	35	1	;	1 1	1	1	1	11	;	1	1 1	}	::	:	!	;	:	!	11	1
SCLIUS. SCHOOL 105	HENT OF I	0	C 1-	1	;	25	50	;	47	;	•	;	11	;	<b>;</b>	• •	•	: :	1	•	1	1	;	37	;
SCLIDS SCIM OF SCIN OF DIS- TUENTS, SOLVE DIS- PFR (TO301) (T0302) 1969 132 19. 1970 1970 1971		ATER	<b>∵</b> •	;	;	16	39	;	36	i	;	;	; ;	;	!	• (	<b>}</b>	: :	;	;	;	•	:	27	;
SCLIDS SCIM OF SCIN OF DIS- TUENTS, SOLVE DIS- PFR (TO301) (T0302) 1969 132 19. 1970 1970 1971	17E0 STAT 152771		SOLIDS DIS- SOLVE (TONS PER AC-FT	•	ł	ł	1	i i	60.		ť		: :			1 -	<b>91</b> •	6 1	60.	1	•14	!	!	116	!
SOL 183 SOM OD SOL 181 1969 1969 1970 1970	Š		SOLIDS, 015- 50LVED (TONS PFR DAY) (70302)	19.6		!	1	ł	540	<b>:</b>		~	: :	ł	91.1		701	i	38	:	41.6	ł		38.2	ł
ш			SOL 155. SUM OF COUSTI- TUENTS, DIS- SOLVED (MG/L) (70301)	13	;	;	;	1	89	}	1	-	11		2	1 6		x	9	<b>!</b>	0 1	ı	:	<b>~</b> 1	:
			⋖	~ :	:	-	_	:	_	06C	: -	•	• •	_		_	_			001	•	: -	:		21

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

	SEDI- MENT. DIS- CHARGE. SUS- PENDED (T/DAY)	1	6.9	729	672	100	7950	3,3	•	40	0.5	16	29	:	113	1	98	: "	• 3	7.0	63	280
,	SEDI- MENT. SUS- PENDED (MG/L)	i	54	272	150	26	1002	10	1	16	81	21	9°	;	45	•	94	1 4	D	6	193	145
	180N (UG/L AS FE) (71885)	370	;	•	!	;	160	;	10	•	!	70	100	4 0	-1	0	1	; ;	•	;	! !	1
	MANGA- NESE (UGZL AS MN)	ł	;	;	1	;	° ¦	;	20	1	!	! 0	10	9 6	•	0	!	1	! !	1	::	!
DATA	NITRO- GEN. NITRATE DIS- SOLVED (MG/L AS NO3)	1.6	;	ł	1	!	8.	!	1.4	!	1	8.0	1 9	04.	:	• 30	;	1.2	;	1	1.6	!
UALITY	NITRO- GEN, AMMONIA DIS- SOLVED (MG/L AS NH4)	1	1	;	;	1	11	;	1	1	!	100	1 1	1	1	1	1	1	<b>ì</b>	1	::	1
	SED. SUSP. FALL DIAM. % FINER THAN 2.00 MM	1	;	;	ł	ľ	100	;	;	1	;	::	1 1		;	;	;	:	:	;	::	1
	SED. SUSP. FALL DIAM. % FINER. THAN 1.00 MM	ľ	;	1	;	i	100	;	;	!	;	11	1 1		ł	;	:	i	:	1	::	;
	SED. SUSP. FALL DIAM. % FINER THAN (70345)	;	;	100	100	ļ	<b>6</b> ;	;	!	;	i	; ;	1	<b>!</b>	100	;	100	1	!	;	100	100
	SUSP. SUSP. FALL DIAM. & FINER THAN. 250 MM	1969	•	96	ው የ	100	97	;	970	1	1	::	; ;		95	1	φ <sub>0</sub>	:	971	!	1 d	Q a
	OATE	MAR . 1	APR 29	MAY 27	الالا 15.	AUG	00.1 07.1		~ .	APR 29		21	16.	JUL 22	200	AUG 28	78 073			10. M	5 6	JJN 2

UNITER STATES DEPARTMENT OF INTERIOR - GFOLOGICAL SURVEY 15277100 - EAGLE P AT EAGLE RIVER AK

WATER QUALITY DATA

							_					_		_
CARBON DIOXIDE DIS-	CMG/L	AS CO2)	0	•	1	1.3	3.4	1.4	15	1	4.2	1	i	1
ם מ	=	(O0400)	ď	; ;	;	8.0	7.7	9.0	9.9	:	7.6	1	7.1	7.4
OXYGEN.	SOLVED	(MG/L)	;	;	;	:	;	1	•	ì	}	!	;	11.8
SPE- CIFIC CON-	ANCE	(S0000)	133	103	97	173	231	183	7.7	162	227	215	101	170
COLOR (PLAT-	COBALT	(00000)	:	;	i	ł	ហ	0	22	;	ď	;	:	;
TUR	ITY	(011)	1	:	!	;	:	1	i	ç	1	ß	i	;
STREAM STAGE	ABOVE	0ATUM)	;	1	;	!	;	;	;	;	ł	;	<b>6.04</b>	;
STREAM- FLOW+	TANEOUS	(CFS) (00061)	715	3500	3050	304	14	373	1620	346	51	76	1290	378
10 V 10 01 10 V	AREA	(SQ MT)		1	;	192	192	192	192	192	192	192	192	;
- 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ATHRE	(DEG C)	ر ب	9	0.9	3.0	c.	0.6	6.5	ŀ	0	7.0	o•&	7.0
	TIME		971	JUL 1130	1130	1000	972 1100	1100	1200	1100	9 <b>73</b> 1130	1115	974 1630	981 1000
		DATE	JUN . 1	J.C.	AUG 14	0C.T	MAR , 1	000 000	AUG 03	0CT 04	7.5.0.	MAY 08.	12	MAY , 1

UNITED STATES DEPARTMENT OF INTERIOR - GFOLOGICAL SURVEY 15277100 - EAGLE P AT EAGLE RIVER AK

MAGNE- SIUM. DIS- SOLVED (MG/L AS MG)	;	:	;	!	5.4	5.0	1.8	;	5.2	;	:	;
CALCIUM D1S- SOLVED (MG/L AS CA) (00915)	ł	;	1	•	36	27	12	:	34	:	;	;
HARD- NESS. NONCAR- BONATE (MG/L CACO3)	12	;	1	20	54	18	7	;	20	:	;	1
HARU- NESS (MG/L AS CACO3)	<b>9</b>	1	1	85	112	88	37	1	110		!	!
PHOS- PHORUS, ORTHO, DIS- SULVED (MG/L AS P) (00671)	;	ł	;	;	1	ł	.050	;	<.010	1	;	ł
PHOS- PHATE, ORTHO, 0IS- SOLVED (MG/L AS PO4)	i	ŧ	;	i	1	ŀ	•15	1	00.	•	:	:
NITRO- GEN, NO2+NO3 DIS- SOLVED (MG/L AS N)		ł	3	;	;	;	• 02	;	.18	;	i i	;
NITRO- GEN, GEN, NITRATE SOLVED (MG/L AS N)		;	1	:	• 20	•25	;	1	;	;	;	ł
CAR- BONATE (MG/L AS CO3)		1	;	0	0	c	0	1	0	;	;	i
BICAR- BONATE (MG/L AS HCO3)	63	;	1	42	107	85	37	;	105	;	1	;
ALKA- INITY FIELD (MG/L AS CAC03)	52	:	;	65	88	70	30	1	96	;	ł	:
PIN FIR (MC) (MC) (MC)	JUN , 1971	JUL 14	AUG 14	04	30	Z 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 3 • • • 0 0 3 • • • 0 0 3 • • • 0 0 3 • • • 0 0 3 • • • 0 0 3 • • • 0 0 3 • • 0 0 3 • • 0 0 3 • • 0 0 3 • • 0 0 3 • 0 0 0 3 • 0 0 0 3 • 0 0 0 3 • 0 0 0 3 • 0 0 0 0	0.4.	FEB , 1973	0.80	12.	MAT + 1961

UNITED STATES DEPARTMENT OF INTERIOR - GFOLOGICAL SURVEY 15277100 - EAGLE R AT EAGLE RIVER AK

,												
MANGA- NESE. DIS- SOLVED (UG/L AS MN)	;	i	;	;	90	10	30	;	20	;	;	i
IHON. DIS. SOLVED (UG/L AS FE)	:	;	:	;	30	7.0	06	;	4 0	i	;	1
COPPER, 01S- SOLVED (UGAL AS CU) (01040)	;	;	;	;	0	;	!	;	;	;	;	;
SILICA. DIS- SOLVED (MG/L AS SIO2) (00955)	:	1	i	!	8.1	2.7	2.1	;	6.3	:	:	:
FLU0- RIDE. DIS- SOLVFD (MG/L AS F)	ł	;	:	;	•1	£•	0.	;		1	ł	;
SULFATE DIS- SOLVED (MG/L AS SO4)	•	:	!	1	92	19	6.8	1	28	1	!	!
CHL0- RIDE. DIS- SOLVED (MG/L AS CL)	;	1	1	;	2.5	1.8	1.4	1	1.7	;	ł	;
POTAS- STUM. DIS- SOLVED (MG/L AS K) (00935)	i	1	i	:	î.	• 5	Ċ,	;	4.	;	1	:
PERCENT SOUTUM (00932)	1	1	;	;	9	8	7	ļ	7	1	;	;
SONTUM SORP- TION RATIO (00931)	!	;	;		.1	<b>~</b> :		!	5.	;	;	i
SOCTUM, DIS- SOLVED (MG/L AS NA)	;	;	i	i	3,3	3.5	1.2	ŀ	1-7	ł		1
SOI D SOI DATE A	21.00	16	14	04	MAR , 1972 30	19. 19.	AU6 03	00T	FER . 1973	90	JUL • 1974	MAY , 1981

UNITED STATES DEPARTMENT OF INTERIOR - GEOLUGICAL SUMVEY 15277100 - EAGLE R AT EAGLE RIVER AK

,												
SED. SUSP. FALL DIAM. % FINER THAN (10340)	:	58	9	;	:	:	56	;	1	:	;	:
SED. SUSP. FALL DIAM. % FINER THAN .008 MM	:	48	46	;	;	;	:	!	;	1	i	;
SED. SUSP. FALL DIAM. & FINER THAN (70338)	i	43	39	;	;	;	38	;	1	1	;	i
SED. SUSP. FALL DIAM. % FINER THAN .002 MM	:	33	32	!	1	:	54	;		;	;	;
SOL 105. 015. SOL VED (TONS PER AC.FT)	;	ŧ	;	:	.18	.14	• 00	:	• 18	;	;	;
SOLIDS. DIS- SOLVED (TONS PER DAY) (70302)	1	1	;	1	17,3	104	201	;	18.2	:	;	;
SOLIDS, SUM OF CONSTI- TUENTS, DIS- SOLVED (MG/L)	;	;	1	ł	136	103	46	1	132	;	;	1
LITHIUM DIS- SOLVED (UG/L AS LI) (01130)	ł	:	ł	!	0	:	i	ł	ł	;	ł	;
ZINC. DIS- SOLVED (UG/L AS ZN) (01090)	;	;	;	i	C	;	i	;	1	;	;	;
STRON- TTUM. DIS- SOLVED (467L AS SR)	171	1	1	:	290	1	;	•	7.	:		187
: AATĒ	JUN + 1971	JUL.	AUG	001	30	. 60 000	AUG 03.	100		0.80	12	12

i	ELEV. OF LAND	MITRO- GEN+	SED.	SED. SUSP.	SED. SUSP.	SED. SUSP.	SED. SUSP.
	15277100 - EAGLE R AT EAGLE RIVER OK		ΤA	WATER GUALITY DATA	WATER OF		

SEDI-	D15-	CH ARGE .	SUS-	PENDED	(T/DAY)	(56108)		1	13600	4080		7	;	41	433	19	•	1.3	i	:
	SEDI-	MENT.	SUS-	PENDED	(MG/L)	(80124)		•	1440	495	ļ	57	1	41	66	20	;	ហ	:	:
ELEV.	SURFACE	DATUM	(FT.	ABOVE	NGVD)	(15000)		•	;	;	; ;	250.00	250.00	250.00	250.00	250.00	250.00	250.00	250.00	;
MITRO- GFM.	VITRATE	DIS-	SOLVED	(MG/L	AS NO3)	(71851)		!	:	;			06.	1.1	;	i	;	l	1	1
SED.	100	DIAM.	% FINER	NAIL	1.00 MM	(10346)		•	;	100		!	1	;	;	;	;	;	;	1
SED.	F A I	OIAM.	A FINER	ZYI	. 500 MM	(70345)		•	100	66		•	1	100	100	1	;	ţ	;	1
SED.		DIAM	& FINER	THAL	.250 MM	(70344)		;	46	44		! !	1	66	86	;	;	;	;	;
560.	- 18 1	O LAM.	FINER	THAN	. 125 MM	(70343)		;	16	93		:	;	95	88	1	;	:	;	:
SED.	5000 P	O T A M	A FINFR	THAN	.062 MM	(70342)		;	81	85		1	;	86	7.7		;	:	;	;
• 0 C: 0 U: 0 U: 0	- LCOC		MAN TO SE	ZVIL	.031 MM	(70341)	971	:	69	20		:	• • • • • • • • • • • • • • • • • • •	ì	1	•	. 1973	;	1974	1981
					DATE		UN . 1	21	14	J6	CT	0.4	30 • • •	175	1.JG 03•••	04	EB , 1	1AY 08	IUL , 1	

PROCESS DATE IS 12-03-81

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY

AGENCY USGS COUNTY 020		SEDIMENT DISCHARGE (TONS/DAY)		0000 •••• •••	0000 ••••• •••	00000 ***** mmmuno	00000	00000 ••••• mmmm	3 3 4 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
SOUNCE STATE 02	SEPTEMBER 1968	MEAN CONCEN- TRATION (MG/L)	DECEMBER							
STREAM DATUM 250.00	10	NEAN DISCHANGE (CFS)	3	80 75 75 75 87	75 70 70 70 70 70	70 70 70 90 90	100 85 80 80 75	25 7 7 7 8 9 9 9 9	70 70 100 140 2540	,
192.00 DA	YEAR OCTOBER 1967	SEDIMENT DISCHARGE (TONS/DAY)		30 30 10 10 10 10	\$0499 00000	mm400	6.0. 7.0 8.0	20 20 10 7.0 6.0	NN 4 4 W 98 O	•
E RIVER AK NPAINAGE AREA	DAY), WATER	MEAN CONCENT TRATION (MG/L)	NOVEMBER							
AT EAGLE RIVER AK NRAINAGE A	SUSPENDED (TONS/DAY).	MEAN DISCHAPGE (CFS)		334 273 208 197 167	115 85 75 70 70	70 70 80 100 110	115 120 130 150 170	216 208 186 117 110	39   8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	ı
0 EAGLE H 1493332	ARGE.	SEDIMENT DISCHARGE (TONS/DAY)		100 90 70 50 50	44400 000 000 000	30 30 30 30 30	20 20 20 20 20 20 20 20 20 20 20 20 20 2	20 20 20 10	30 20 20 20 20 20 20 20 20 20 20 20 20 20	•
15277100 LONGITUDE	SEDIMENT DISCH	MEAN CONCEN- TRATION (MG/L)	OCTORER		!!!!!		!!!!!	!!!!!		
STATION MUMBER LATITUDE 611829		MEAN DISCHARGE (CPS)		5322 444 449 413	367 352 340 326 316	302 288 284 277.	260 248 226 225 219	229 226 213 189 157	254 208 190 222 227	
STATIC		₽¢Q		⊣ ഗ.യ 4 N	<b>6</b> 6 6 0 1	113	61 18 19 05	222	26 27 29 29 30 31	

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY

PROCESS DATE IS 12-03-81

4 SOURCE AGENCY USGS	STATE 02 COUNTY 020
STREAM	250.00
	DATUM
	192.00
EAGLE R AT EAGLE PIVER AK	NPAINAGE AREA
EAGLE	1493332
15277100	LONGITUDE
STATION WUMBE	LATITUDE 611828

STATION N LATITUDE	STATION MUMBE LATITUDE 611828	15277100 LONGITUDE	EAGLE R 1493332	AT EAGLE PIVER NRAINAG	E PIVER AK Npainage area	192.00 DA	STREAM DATUM 250+00	IAM SÖURCE	AGENCY USGS COUNTY 020
		SEDIMENT DISCHARGE.	SCHARGE, SUSP	ENDED (TONS/	DAY), WATER	SUSPENDED (TONS/DAY), WATER YEAR OCTUBER 1967	2	SEPTEMBER 1968	
<b>&gt;</b>	MEAN DISCHARGE (CFS)	NEAU CONCEN- TRATION (MG/L)	SFUIMENT DISCHARGE (TONS/DAY)	MEAN DISCHARGE (CFS)	MEAN CONCEN- TRATION (MG/L)	SEDIMENT DISCHARGE (TONS/DAY)	MEAN DISCHARGE (CFS)	MEAN CONCEN- TRATION (MG/L)	SEDIMENT DISCHARGE (TONS/DAY)
		JANUARY			FEBRUARY			MARCH	
ለ m 4 ID	11 955 95 85 85		@ 40 N 4 4 0 0 0 0 0 0	00000 LLLLLL		00000	0 0 0 0 0 0 0 0 0 0		00000
9788G	2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3		8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	<b>6666</b> 6		00000	00000		00000
T.E. 450	00000 0000 0000 0000		00000	00000 20000		00000	00000		00000
21 18 19 20	ភ <b>៤ ១ ១ ១</b> ស ស ស ស ស		00000	00000 02000		00000	00000		00000
21 22 22 24 25	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$		00000	00000 0000		cc000	00000		00000
4 K B B B B B B B B B B B B B B B B B B	<b>ራ</b> æ æ æ æ æ ሚኒስር ሲያ		000000	~~~~!! ••••!!		0000	000000		000000
TOTAL	2220		Đ•3•0	1843		44.0	1880		31.0

PRUCESS DATE IS 12-03-81

UNITED STATES DEPARTMENT OF THTERIOR - GEOLUGICAL SURVEY

SOURCE AGENCY USGS STREAM 15277100 EAGLE R AT EAGLF RIVER AK STATION NUMBER

COUNTY 020		SEDIMENT DISCHARGE (TONS/DAY)		46844 4686 468	27 22 32 32 48	257 679 772 704	685 284 254 254	239 188 157 129	146 127 105 773	1400
STATE 02	SEPTEMBER 1968	MEAN CONCEN- TRATION (MG/L)	JUNE	233 33 33 33 33	17 15 20 27	53 105 215 220 185	135 130 84 80	<b>~ 6.6</b> € ∨ 0.00 € ∨ 0.00 € 0	6 4 5 5 1 1 2 5 0 3 8 5 1 1 1 2 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1	;
UM 250.00	1967 TO SEPT	MEAN DISCHARGE (CFS)		698 638 621 590 579	579 570 560 585 656	773 906 1170 1300	1450 1290 1170 1120	1180 1070 970 866 843	986 978 1090 1380 1590	28818
192.00 DATUM	YFAR OCTOBER	SEDIMENT DISCHARGE (TONS/DAY)		44WW0	7.0 7.0 8.0 8.0	10 10 20 40 40	30 30 40 50	230 402 331 253 189	159 122 102 316 450 219	3217.0
SE AREA	WATER	MEAN CONCEN- TRATION (MG/L)	MAY	11111	9         9	11111	11111	242 175 130 96	80 65 55 140 207 95	;
DRAINAGE	SUSPENDED (TONS/DAY),	MEAN DISCHARGE (CFS)		88 88 ዓ ዓ ዓ ዓ	95 100 105 110 115	12n 138 169 205 224	225 224 247 287 310	500 615 700 720 730	736 698 686 835 833 855	11047
1493332	ARGE,	SEDIMENT DISCHARGE (TONS/DAY)			00000			00000 NNNN	W W W 4 4 0 0 0 0 0 0	48.0
LONGITUDE	SEDIMENT DISCH	MEAN CONCEN- TRATION (MG/L)	APHIL							
STATIONE BOOMER	·	MEAN DISCHAPGE (CFS)		0 C S O O	0000 <b>0</b>	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	66663 66669	64.64.64 R 22.04.04.04	20022	1894
LATITU		Y A C		የመመ 4 መ	6 L C C C C	12.E48	511 711 90 00	22 22 25 25 25	25 25 25 25 25 25 25 25 25 25 25 25 25 2	TOTAL

UNITED STATES DEPARTMENT OF INTERIOR - GEOLUGICAL SURVEY

PRUCESS DATE 15 12-03-81

STREAM SOURCE AGENCY USGS 192.00 DATUM 250.00 STATE 02 COUNTY 020 15277100 FAGLE R AT EAGLF RIVER AK LONGITUDE 1493332 DRAINAGE APEA STATION NUMBER LATITIOE 611828

SEDIMENT DISCHANGE, SUSPENDED (TONS/DAY), WATER YEAR OCTOBER 1967 TO SEPTEMBER 1968

SEDIMENT DISCHARGE (TONS/DAY)		150 120 120 100	220 200 160 100 58	4.14 3.88 3.66	30 23 16 17	11 10 7.59 7.58	484661 ••••••	1801.4
MEAN CONCEN- TRATION (MG/L)	SEPTEMBER	73 644 57 92	90 78 46 30 30	400 mm	30 25 20 20 20 20	21 22 24 44	8 0 8 0 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	;
MEAN DISCHARGE (CFS)		773 704 668 650 780	898 962 914 829 710	54 730 730 704 704	376 336 317 303 282	243 243 233 230	222 222 222 222 222 222 222	14271
SEDIMENT DISCHARGE (TONS/DAY)		640 519 384 399 456	1260 1860 1660 1410 1010	803 653 677 607 470	385 324 344 453	813 388 220 280 469	280 240 314 240 180 170	18210
MEAN CONCEN- TRATION (MG/L)	AUGUST	150 130 106 107 109	240 298 268 230 175	172 155 151 148 132	108 100 100 101	172 105 70 85 155	95 88 120 95 74 72	) † †
MEAN DISCHARGE (CFS)		158n 148n 134n 138n 1550	1950 2310 2290 2270 2130	1730 1560 1660 1520 1320	1320 1200 1120 1260 1510	1750 1370 1190 1220 1120	1100 1010 970 954 914 958	44936
SEDIMENT DISCHARGE (TONS/DAY)		903 792 598 483 520	688 874 1780 2540 1730	969 656 524 539 555	578 661 616 526 579	642 709 980 1100 1340	1690 1850 1490 1350 1040	30074 62313.4
MEAN CONCEN- TRATION (MG/L)	JULY	198 180 143 125 125	150 175 320 417 315	215 149 122 121	138 140 130	135 150 190 230 260	285 325 295 250 182 158	
MEAN DISCHARGE (CFS)		1690 1630 1550 1430 1540	1700 1850 2060 2260 2030	1670 1630 1590 1650	1550 1610 1630 1500 1650	1760 1750 1910 1770 1910	2200 2110 1870 2000 2110	55040 177409
747		0° E 4 D	0 r s 6 0	113	2118 200 200	22 23 24 24 25	26 77 82 92 93 11	T014L YF 4R

NOTE: MUMBER OF MISSING DAYS OF RECORD EXCEEDED 20% OF YEAR

PRUCESS DATE IS 12-03-81

UNITED STATES DEPARTMENT OF INTERIOR - GEOLUGICAL SURVEY

SEDIMENT DISCHARGE (TOMS/DAY) SOURCE AGENCY USGS STATE 02 COUNTY 020 41.49 888888 81 81 81 81 74 91119 00000 SEDIMENT DISCHARGE, SUSPENDED (TONS/DAY), WATER YFAR OCTOBER 1968 TO SEPTEMBER 1969 MEAN CONCEN-TRATION (MG/L) DECEMBER •••• ហេហេហេហ លេខខាលខាល STREAM 250.00 MEAN DISCHARGE (CFS) 80 72 60 60 60 65 65 65 65 65 500000 DATUM SEDIMENT PISCHARGE (TONS/DAY) 4444 20000 20000 192,00 MEAN CONCEN-TRATION (MG/L) NOVEMBER DRAINAGE AMEA 15277100 EAGLE R AT EAGLE RIVER AK LONGITUDE 1493332 MEAN DISCHARGE (CFS) 120 100 1000 3195 SEDIMENT DISCHARGE (TONS/DAY) 8.9 24 24 17 29 26 14 8•9 120 86.0 44.0 45.004 7.0 6.8 7.5 8.1 316.7 MFAN CONCEN-TRATION (MG/L) OCTORER 19 13 13 13 13 13 13 50000 STATION NUMBER LATITUDE 611828 DISCHARGE (CFS) MF A N 201 192 194 189 158 152 119 119 135 130 130 125 125 161 164 162 130 125 150 150 4810 6000 PAY

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY

PROCESS DATE IS 12-03-81

		· .								
AGENCY USGS COUNTY 020		SEDIMENT DISCHARGE (TONS/DAY)		66666	gonne	eeeeee		4444 8 8 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	444600 444600	11.90
SOURCE STATE 02	SEPTEMBER 1969	MEAN CONCEN- TKATION (MG/L)	MARCH	ммммм	ଅଟମ ଅଟନ <sub>୍</sub>	ଅଟମ ପଟନ	ппппп	44444	44444	į
STREAM TUM 250.00	10	MEAN DISCHARGE (CFS)		366 366 366 366	366 388 388 388	8 8 8 8 8 8 8 8 8 8	8 7 8 0 0 0	44444 04444	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1289
192.00 DATUM	YEAR OCTOBER 1968	SEDIMENT DISCHARGE (TONS/DAY)		7,7,2,2,2,2,2,2,2,2,2,2,2,2,2,2,2,2,2,2	7,7,7,7,1 1,7,7,7,1	55 55 55 55 55 55 55 55 55 55 55 55 55 55	35 35 35 35 35 35 35 35	8 8 8 8 8	25.58 11.58 11.58	7.24
F RIVEH AK Orainage area	CTONSZUAY), WATER	MEAN CONCEN- TRATION (MG/L)	FEBRUARY	ппппп	ппппп	папап	ппппп	ппппп	mmm	1 1 2
AT EAGLE RIVER DRAINAGE	SUSPENDED (TONS/	MEAN DISCHARGE (CFS)				& & & & & & & & & & & & & & & & & & &	88888 8888	44444 44444	444111 mmm111	268
EAGLE R 1493332	E.	SFOIMENT DISCHARGE (TONS/DAY)			99444 666666	88888 8888 1888 1888		29 29 28 28 88 88	66666666666666666666666666666666666666	10.37
15277100 LONGITUDE	SFDIMENT DISCHARG	MEAN CONCEN- TRATION (MG/L)	JANUARY	<b>च</b> चचचच	<b>~~~</b>	m m m m m	<b></b>		<i>ପ ପ ପ ପ ପ</i> ପ ପ	;
STATION NUMBER LATITODE 611828		MEAN DISCHAMBE (CFS)		ພພ444 ນິຣິ໖໕4	4444 44060	4444W 5056Q	######################################	999444 99444	**************************************	1199
STATION I		DAY		ተለመታወ	<b>6≻</b> 800 100	1122 132 133 134 135	271116 000	288848 48848	92000E	TOTAL

PROCESS DATE IS 12-03-81	STREAM SOURCE AGENCY USGS 192.00 DATUM 250.00 STATE 02 COUNTY 020
VEY	STREAM 250.00
ICAL SUR	DATUM
R - GEOLUG	192.00
UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY	R AT EAGLE RIVER AK 2 DRAINAGE AREA
TEO STATE	EAGLE R 1493332
INU	15277100 EAGLE LONGITUDE 1493332
	STATION NUMBER LATITURE 611828

SFDIMENT DISCHARGE, SUSPENDED (TONS/DAY), WATER YEAR OCTOBER 1968 TO SEPTEMBER 1969

SEDIMENT DISCHANGE (TONS/DAY)		8444RR 8444RR	34 46 72 177 162	112 204 334 488 726	4070 4190 1300 925	761 699 575 398 547	932 1150 1220 1130 23798
MEAN CONCEN- THATION (MG/L)	JUNE	998 988 988 988	4 6 4 8 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	46 72 103 138 165	668 360 298 233	200 185 149 110	217 242 252 247 226
MEAN DISCHARGE (CFS)		4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	520 535 632 773 882	898 1050 1200 1310 1630	2210 2350 1890 1620 1470	1410 1400 1430 1340	1590 1760 1890 1850 1860
SEDIMENT DISCHARGE (TONS/DAY)		40000 40000	7.0 7.6 7.6 8.1 8.1	\$ \$ \$ \$ \$ \$ \$	15 15 32 61 51	39 334 369 207 296	473 664 251 124 124 140
MEAN CONCEN- TRATION (MG/L)	MAY	20 20 20 20 20 20	60000 44444	20 20 20 20 20	33 32 53 106 72	52 249 280 150 170	190 232 115 75 80 100
MEAN DISCHARGE (CFS)		110 110 120 120	130 140 150 150	160 150 170 170	172 175 186 212 261	276 416 515 510 644	922 1060 808 614 575 520 9996
SEDIMENT DISCHARGE (TONS/DAY)		4.00.00.00.00.00.00.00.00.00.00.00.00.00		 5	~~~~~ ~~~~~~	ଅପ୍ୟସ୍ଥ ବ୍ୟବ୍ୟସ	8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1
MEAN CONCEN- TRATION (MG/L)	APRIL	ហមកម្មា	<u> </u>	σε ασιασιασιασι	110001	2.00 2.00 2.00 2.00 2.00 2.00 2.00 2.00	2 8 8 3 3 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
MEAN DISCHARGE (CFS)		22 C C C C C C C C C C C C C C C C C C	1000 1000 1000	7 7 7 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7	ແ ແ ແ <b>ແ</b> c ວ ວ ນ <b>ທ</b>	58 00 00 00 00 00 00 00 00 00 00 00 00 00	95 100 105 105 105
944		-064s	67 8 9 10 10 10 10 10 10 10 10 10 10 10 10 10	1130	15 11 19 20	22 22 24 25 25	256 259 310 1410 1410

PROCESS DATE 1S 12-03-81

UNITED STATES DEPARTMENT OF INTERIOR - GEOLUGICAL SUMVEY

SOUNCE AGENCY USGS 192.00 DATUM 250.00 STATE 02 COUNTY 020 15277100 EAGLE R AT EAGLF RIVER AK LONGITUDE 1493332 DRAINAGE AREA STATION NUMMER INTINUE STIAZE

SEDIMENT DISCHARGE, SUSPENDED (TONS/DAY), WATER YEAR OCTOBER 1968 TO SEPTEMBER 1969

	99	2;	4	9.	?; <b>₹</b>	30	88	88	27	ñ	207	160	99	S •	3	39	53	27	50	20	<b>26</b>	31		7 S		9 -		M	11	;	1336.6	
SEPTEMBER	66	010	37	37	35	56	56	56 26	26 	u F	95	76	45	9 1	37	32	56	92 7	52	21	56	28	58	26 21	i i	50.	9 5	14	12	1	i	
	626	999	770	602	6 % 4 C	432	<b>404</b>	404	388	000	808	780	585 5	510	4 / v	450	408	384	372	356	372	412	408	304 324	: ;	296	267	356	348	:	13711	
	6	σ,	N	4 (	າ	785	593	437	300	007	230	154	115	62	7	68	9	85	. 83	96					· ·	9 <u>7</u>	0 F	2.5	9/	77	6805	
AUGUST	<b>7</b> 00	<b>~</b> 1	2	N I	•	9	S	m	(	<b>&gt;</b>	87	29	61		84	46	245	64	4	56	32	37	34	7 7 7 7 9 7 9	. !	ທ - ທ ເ	1 4 7 d	37	(A)	4.5	;	
	1310	1370	1520	1560	0002	1730	1390	1190	1010	<b>*</b>	978	92V	869	550	545	545	575	959	63A	63я	632	608	575	4 8 0 0	,	515	0.0 919	029	674	632	25072	
	923	767	812	1020	706	906	974	404	619	573	476	964	555	695	663	516	443	4	4	366	345	325	358	1100		742	5.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	. ur	320	312	18929	54783,08
JULY	191	168	178	200	002	194	184	161	145	۲۵.	116	110	123	147	147	121	116	112	105	102	76	26	76	147	) 					80	ļ	
	1790	1690	69	89	2	1730	1760	1630	1580	0561	52	19	67	75	67	58	43	47	7	33	36	31	47	51 86		47	700	57	7	30	48440	152739
	-	2	m	<b>4</b>	ī.	¢	~	œ								16	17	13	19	50	21	22	23	ን የ ት ቤ	) J	96	~ 0	5 O	` @ M	1,0	TOTAL	YEAR
	AUGUST	JULY AUGUST SEPTEMBER 1790 191 923 1310 84 297 626 39 6	JULY AUGUST SEPTEMBER 1790 191 923 1310 84 297 626 39 6 1690 168 767 1370 79 292 668 40 7	JULY AUGUST SEPTEMBER  1790 191 923 1310 84 297 626 39 6 1690 168 767 1370 79 292 668 40 7 1690 179 812 1520 128 525 644 37 6	JULY AUGUST SEPTEMBER  1790 191 923 1310 84 297 626 39 6 1690 168 767 1370 79 292 668 40 7 1690 178 812 1520 128 525 644 37 6 1890 200 1020 1560 154 649 602 37 6	AUGUST 923 131n 84 297 626 767 137n 79 292 668 812 152n 128 525 644 1020 1560 154 649 602 967 2000 173 934 495	JULY AUGUST AUGUST SEPTEMBER  1790 191 923 131n 84 297 626 39 6 1690 168 767 137n 79 292 668 40 77 1690 1791 1520 1520 1580 154 644 37 6 1890 200 1020 1560 154 649 602 37 6 1790 200 967 2000 1730 168 785 432 26 3	JULY  1790 191 923 131n 84 297 626 39 6 1690 1781 1370 79 292 668 40 77 1690 1781 1520 1580 1584 602 37 6 1890 200 1020 1560 154 649 602 37 6 1790 200 967 2000 1730 168 785 432 26 2	JULY  AUGUST	JULY  AUGUST  AUGUST  AUGUST  AUGUST  AUGUST  AUGUST  AUGUST  SEPTEMBER  SEPT	JULY  AUGUST	1         1790         191         923         131n         84         297         626         39         6           2         1690         168         767         137n         79         292         668         40         7           3         1690         168         767         137n         79         292         668         40         7           4         1690         168         767         1520         158         644         37         6           5         1790         200         1560         173         934         495         32         4           6         1730         194         906         1730         168         785         432         26         26         2           7         1760         184         874         139n         168         793         404         26         2	1         1790         191         923         131n         84         297         626         39         6           2         1690         168         767         137n         79         292         668         40         7           3         1690         168         767         137n         79         292         668         40         7           4         1690         178         168         767         1560         156         37         6           4         1690         200         1620         1560         156         37         6         37         6           4         1890         200         1560         173         164         495         32         46         495         33         46         495         32         46         26	1   1790     191     923     1310     84     297     626     40     7       2   1690     168     767     1370     79     292     668     40     7       3   1690     168     767     1370     178     649     664     37     6       4   1690     178     1620     1560     1560     157     649     602     37     6       4   1690     200     1020     1560     173     168     765     649     602     37     6       5   1790     194     906     1730     168     785     495     32     26     26       6   1730     161     709     1190     136     785     404     26     26     26     26       7   1760     161     709     1190     136     437     404     26     <	JULY  AUGUST  AUGUST  AUGUST  AUGUST  AUGUST  AUGUST  SEPTEMBER  S	1         1790         191         923         131n         84         297         626         39         6           2         1690         168         767         137n         79         292         668         40         7           3         1690         168         767         137n         79         292         668         40         7           4         1690         178         156         156         49         668         40         7           4         1690         178         156         649         662         37         6           5         1790         1920         156         495         33         40         26         37         6           6         1730         194         967         178         495         495         36         26         26         33         404         26         26         26         26         26         26         26         37         404         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26         26	JULY         AUGUST         SEPTEMBER           1   1790         191         923         1131n         84         797         626         39         648         40         77         137         128         292         668         40         77         137         128         292         668         40         77         137         128         292         668         40         77         137         128         292         668         40         70         77         137         128         292         668         40         77         74         140	JULY         AUGUST         SEPTEMBER           1 1790         191         923         131n         84         292         668         40         7           2 1690         168         767         137n         79         292         668         40         7           3 1690         168         767         137n         178         292         664         40         7           4         1690         168         767         137n         178         292         664         40         7           4         1690         107         136         173         649         662         37         66         40         7         4	JULY  AUGUST	JULY  AUGUST	1790   191   923   1310   84   297   626   39   64   40   64   64   64   64   64   64	1790	1 1700         191         923         131n         84         297         626         39           2 1690         169         168         167         137n         179         292         668         40           4 1690         178         167         152n         152         668         40           4 1690         200         1020         1560         173         668         40           5 1700         200         1020         1560         173         669         602         37           6 1730         184         906         173n         168         785         432         26           7 1760         184         906         173n         168         785         432         26           8 1540         161         170         119         496         173         437         404         26           1 1540         164         906         173n         168         73         404         26         26           1 1540         164         906         173n         110         110         110         256         437         404         26           1 1570         116	1790         191         923         131n         84         297         626         39           2         1690         168         767         137n         79         292         664         37           3         1690         168         767         137n         129         5292         664         40           4         1690         173         1920         156         173         40         40         40         40         40         40         40         40         26         40         40         26         40         31         31         31         31         32         31         31         32         32         40         26         40         31         31         32         32         40         26         40         31         31         32         32         40         40         26         40         26         40         30         31         40         26         40         40         26         40         30         30         38         40         40         26         40         40         40         40         40         40         40         40         40	11790         191         923         131n         84         297         626         39           2         1690         168         767         137n         179         292         664         37           4         1690         176         1170         173         194         906         173         173         934         495         37           4         1690         200         1020         1560         173         168         785         644         37         32           4         1790         200         173         168         785         649         37         32<	1790   191   923   1310   84   297   626   399   64   64   64   64   64   64   64	1790	1790	1790	1700   191   923   1310   94   297   668   40   40   40   40   40   40   40   4	170   191   767   131   794   292   668   40   767   767   137   794   292   668   40   767   767   794   793   794   668   40   767   767   794   693   694   495   794   694   495   794   694   495   794   694   495   794   694   495   794   694   495   794   694   495   794   694   495   794   694   495   794   694   495   794   694   495   794   694   4	1910   1911   1912   1922   1924   6464   409   765

PHOCESS DATE IS 12-03-81 UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY

/ USGS		SEDIMENT DISCHARGE (TONS/DAY)							;	
AGENCY USGS COUNTY 020		SEDIM DISCH								
SOURCE STATE 02	SEPTEMBER 1970	MEAN CONCEN- TRATION (MG/L)	DECEMBER							
STREAM 250.00	10	MEAN DISCHARGE (CFS)		120 120 120 120	120 120 120 120 120	120 120 120 120	120 120 120 130 130	130 120 120 120 120	110 110 110 110 110 120	3700
DATUM	R 196									Ю
192,00	YEAR OCTOBE	SEDIMENT DISCHARGE (TONS/DAY)								
A AK GE AREA	DAY), WATER	MEAN CONCEN- TRATION (MG/L)	NOVEMBER							
AT EAGLF RIVFR A	F, SUSPENDED (TONS/DAY), WATER YEAR OCTOBER 1969	MEAN DISCHARGE (CFS)		327 340 300 270 250	230 210 200 190	170 160 150 150	1440 1460 1360 1360	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	130 120 120 120	5210
EAGLE R 1493332	CHARGE, SUSP	SEDIMENT DISCHARGE (TONS/DAY)								
15277100 LONGITUDE	SEDIMENT DISCHARG	MEAN CONCEN- TRATION (MG/L)	OCTORER							
STATION NUMBER LATITUDE 611828		MEAN DISCHAPGE (CFS)		389 275 312 366	784 2746 1460 1460 1040	1170 1370 1340 1340 943	754 656 644 570 485	4338 326 303 885	2233 2233 2233 2233 2333 2333	21924
STAFID		<b>,</b> ∨ C		⊸ (v m a li)	9re001	13821	179 179 20	70078 -0048	200 200 300 310	TOTAL

PROCESS DATE IS 12-03-81

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY

SOURCE AGENCY USGS STATE 02 COUNTY 020
STREAM 250.00
DATUM
192.00
00 EAGLE R AT EAGLE RIVER AK E 1493332 APEA
EAGLE R 1493332
15277100 LONGITUDE
STATIOM NURBER LATITUDE A11828

SFOIMENT DISCHARGE, SUSPENDED (TONS/DAY), WATER YEAR OCTOBER 1969 TO SEPTEMBER 1970

SEDIMENT DISCHARGE (TONS/DAY)							
MEAN CONCEN- TRATION (MG/L)	MARCH						
MEAN DISCHARGE (CFS)		00000	89 89 89 89 89 89 89 89 89 89 89 89 89 8	8 8 8 8 8 ទ ព ព ព ព	90 90 90 90 90 90 90 90	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	80 80 80 80 80 80
SEDIMENT DISCHARGE (TONS/DAY)							
MEAN CONCEN- TRATION (MG/L)	FEBRUARY					V	
MEAN DISCHARGE (CFS)		00000	00000	66666	00000	000,00	252 252
SEDIMENT DISCHARGE (TONS/DAY)							
WEAN CONCENT TRATION (MG/L)	JANUARY						
MEAN DISCHAHGE (CFS)		120 110 110 110	100 100 100 100	100 100 100 100 100	955 955 955 955	995 995 995 995	955 955 95 95 95
			9re001	11122	\$ P & B B O	7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	26 23 30 31

PROCESS DATE IS 12-03-81

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY

STATE 02 COUNTY 020	SEPTEMBER 1970	MEAN CONCEN- SEDIMENT TRATION DISCHAMGE (MG/L) (TONS/DAY)	JUNE							
STREAM DATUM 250.00	1969 TO	MEAN DISCHARGE (CFS)		360 370 400 450	410 500 800 700 600	700 800 1000 800 700	662 698 728	754 775 845 929 1010	964 985 1120 1210 1150	22180
192.00 D	YFAH OCTOBER	SEDIMENT DISCHARGE (TONS/DAY)								
F RIVER AK DRAINAGE AREA	(TONS/DAY), WATER	MEAN CONCENT TRATION (MG/L)	МАХ							
AT EAGLE RIVER AK DRAINAGE A	SUSPENDED (TON	MEAN DISCHARGE (CFS)		0 X & 9 &	86 94 96 98 106	127 165 202 267 288	276 267 255 255 264	279 291 291 294 285	288 329 366 366 350	6757
100 EAGLE R JE 1493332	RGE,	SEDIMENT DISCHARGE (TONS/DAY)								
15277100 LONGITUDE	SEDIMENT DISCHA	MEAN CONCEN- TRATION (MG/L)	APRIL							
STATION NUMBER LATITUDE 611828		MEAN DISCHAPGE (CFS)		000000 000000	0 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	# # # # # # # # # # # # # # # # # # #	27 27 27 27 27	75 75 75 75 75	77 79 81 82	1387
STATION O		740		W # 4 # #	6 × 4 & 0	11 12 14 15	16 17 19 20	22222	22 23 33 31	TOTAL

PHUCESS DATE IS 12-03-81

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY

STREAM SOURCE AGENCY USGS 250.00 STATE 02 COUNTY 020 192.00 DATUM 19277100 EAGLE R AT EAGLE RIVER AK LONGITUDE 1493332 OPAINAGE AREA STATION NUMBER I ATTIONE 611928

	SEDIMENT DISCHARGE (TONS/DAY)								
SEPTEMBER 1970		SEPTEMBER							
			803 776 775 957	728 6332 530 458 430	6 4 4 4 6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	761 698 686 620 535	470 428 390 362 352		17636
YEAR OCTOBER 1969 TO	SEDIMENT DISCHARGE (TONS/DAY)								
		AUGUST							
SUSPENDED (TONS/DAY), WATER	MEAN DISCHARGE (CFS)		2090 1820 1700 1450	1590 1740 1640 1330	1150 1280 1440 1350	1290 1210 1250 1310	1090 1090 985 866 782	761 787 789 810 838 845	3846A
									165838
SPOIMENT DISCHARGE.	ME AN CONCEN- TRATION (MG/L)	JULY							
	MEAN DISCHAPGE (CFS)		1180 1240 1310 1340 1310	1180 1080 1160 1390 1310	1230 1230 1200 1140	971 936 1040 1050 971	1010 1010 971 999 1150	1390 1750 2060 2110 2370	40378 166338
	<b>}</b> v C		<b></b> 000410	& <b>C</b> & & & O	10646	20 20 20 20	22 23 24 25 25	25 25 25 30 31	TOTAL. YFAR

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY

PRUCESS DATE IS 12-03-81

AGENCY USGS COUNTY 020		SEDIMENT Discharge (Tons/Day)								
SOURCE A STATE 02	TO SEPTEMBER 1971	MEAN CONCEN- TRATION (MG/L)	DECEMBER							
STREAM DATUM 250.00	1970 TO SEPT	MEAN DISCHARGE (CFS)		8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8 8 8 8 8 8 8	78 78 87 87 87	37 36 37 37 37	44440 44440	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2320
192.00 DA	YEAR OCTOBER 1970	SEDIMENT PISCHARGE (TONS/DAY)								
F RIVER AK DRAINAGE AREA	E, SUSPENDED (TONS/DAY), WATER	MEDN CONCEN- TRATION (MG/L)	NOVEMBER							
AT EAGLE RIVER AK PRAINAGE A	PENDED (TONS	MEAN DISCHAPGE (CFS)		160 120 110 130	140 130 115 115	105 100 98 96 94	00 00 00 00 00 00 00 00 00 00 00 00 00	8 8 8 8 8 4 4 4 4	9 9 8 8 8 6 1 4 4 5 5 5 5 1	3086
EAGLE R 1493332		SEDIMENT OISCHARGE (TONS/DAY)								
15277100 LONGITUDE	SFDIMENT DISCHARG	MEAN CONCEN- TRATION (MG/L)	OCTORER							
STATION NUMBER LATITUDE 611828		MFAN DISCHAMGE (CFS)		300 300 297 264 31	255 249 230 220 210	2000 1900 170 173	153 151 155 135 80	1120 110 100	100 110 130 160 180	5599
STATION :		Ç		⊸~~4 <i>w</i>	3 t & 6 0 1		20 C	22222	330	TOTAL

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY

STHEAM SOURCE AGENCY USGS 192.00 DATUM 250.00 STATE 02 COUNTY 020 15277100 EAGLE R AT EAGLE RIVER AK LONGITUDE 1493332 DRAINAGE AREA STATION NUMBER LATITUDE 611828

	SEDIMENT DISCHARGE (TONS/DAY)								
SEPTEMBER 1971	MEAN CONCEN- TRATION (MG/L)	MARCH							
10	MEAN DISCHARGE (CFS)		4444 90044	88888 88888	144 100 000	6 6 6 6 6 6 6 6 6	88888	33.4	1244
YEAR OCTOBER 1970	SEDIMENT DISCHARGE (TONS/DAY)								
RGE, SUSPENDED (TONS/DAY), WATER	MEAN CONCEN- TRATION (MG/L)	FEBRUARY							
ENDED (TONS	MEAN DISCHARGE (CFS)		ດ ດ ດ ດ ລ ທ ທ ທ ທ ທ	™ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ი გ. გ. გ. გ. დ. ტ. გ. გ. გ. წ.	ວວວ <i>ກກ</i> ພະບອນ	044'44 COOKK	444	1456
DISCHARGE, SUSP	SEDIMENT DISCHARGE (TONS/DAY)								
SFDIMENT DI	MEAN CONCEN- TRATION (MG/L)	JANUARY							
	MEAN DISCHARGE (GFS)		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	\$ 4 5 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	တွင် ည ဂူ လ တွင် & ထို ဧ	<b>ՆՆՇՆՆ</b> <b>ՀՀՕ</b> 44	ው ዓ ት ዓ ር ረ ር ዓ ር ረ ር	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	1774
	<b>≻</b> ∧ ∩		N W 4 W	<pre>creec</pre>	1112 127 137 137	2000	1000 1000 1000 1000 1000 1000 1000 100	25 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	TOTAL

PROCESS DATE 15 12-03-81

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY

AGENCY USGS COUNTY 020		SEDIMENT DISCHARGE (TONS/DAY)		457.4	213 249 335 455 708	492 272 282 400 394	218 1167 1103 147	247 167 216 367 718	1330 1280 1080 873 732	11634
SOURCE STATE 02	SEPTEMBER 1971	MEAN CONCEN- TRATION (MG/L)	JUNE	366 246 245	385 385 385 365 400	268 158 155 200 174	110 87 71 72 100	136 90 110 140	300 260 240 220 198	i
STREAM M 250.00	1970 TO SEPTE	MEAN DISCHARGE (CFS)		143 1239 143 163	243 312 382 462 656	680 638 674 740 838	734 626 5336 520 545	674 686 728 971 1400	1640 1820 1670 1470 1370	21737
192.00 BATUM	YEAR OCTOBER 1	SEUIMENT DISCHARGE E (TONS/DAY)								
E RIVEK AK DRAINAGE AREA		MEAN CONCEN- TRATION (MG/L)	МАУ							
AT EAGLE RIVEH DRAINAGE	HARGE. SUSPENDED (TONS/DAY), WATER	MEAN DISCHARGE (CFS)		355 355 475 77	24 20 20 20 20	44000 ഗസരട	55 60 80 120	140 120 120 130	140 133 133 143 139	2546
EAGLE R 1493332		SEDIMENT DISCHARGE (TONS/DAY)								
15277100 LONGITUDE	SEDIMENT DISC	MEAN CONCEN- TRATION (MG/L)	APRIL							
STATION NUMBER LATITUDE 611829		MEAN DISCHARGE (CFS)		mmmm 7 + 7 + +	34 34 34 36 36	38888	32 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	• N2NNNN • N2NNNN • N2NNNNN	1070
STATION LATITUDE		7 8 9		-0r45	& r & e o o	1122451 22451	20 20 20	22 22 24 25 25	22 23 30 31 31	TOTAL

UNITED STATES DEPARTMENT OF INTERIOR - GEOLOGICAL SURVEY

PROCESS DATE IS 12-03-81

STREAM SOURCE AGENCY USGS	DATUM 250.00 STATE 02 COUNTY 020
	192.00 D
AT EAGLE RIVER AK	1493332 NRAINAGE AREA
FAGLE R	1493332
15277190	LONGITUDE
STATION NUMBER	LATITUDE 611828

SFOIMENT DISCHARGE, SUSPENDED (TONS/DAY), WATER YEAR OCTOBER 1970 TO SEPTEMBER 1971

SEDIMENT DISCHARGE (TONS/DAY)								
MEAN CONCEN- TRATION (MG/L)	SEPTEMBER							
MEAN DISCHARGE (CFS)		1290 1220 1050 898 881	804 662 601 564 531	495 471 461 468	4 3 4 5 5 6 4 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6	502 427 380 354	330 307 290 284 277	16570
SEDIMENT DISCHARGE (TONS/DAY)								
MEAN CONCEN- TRATION (MG/L)	AUGUST							
MEAN DISCHAPGE (CFS)		1800 1900 1700 1400 1200	1500 2000 3000 4500 4000	3500 2800 2800 2940 2560	2200 1990 2050 1870 1670	1590 1650 1580 1450	1350 1240 1070 1030 1110	62050
SEDIMENT DISCHARGE (TONS/DAY)		522 404 319 292 334	425 657 1290 1800 3400	4830 4720 14400 15300 7540	4230 2820 2110 1560 2060	1920		70933 82567
MEAN CONCEN- TRATION (MG/L)	JULY	168 129 120 120	130 175 318 405 655	820 725 1810 1650 950	640 500 400 325 365	32	!!!!!!	•
MEAN DISCHANGE (CFS)		1150 1010 922 901 1030	1210 1390 1500 1650	2180 2410 2950 3430 2940	2450 2090 1950 1780 2090	2030 1700 1500 1150	1500 1800 2100 1800 1500	54933 174385
P.A.Y		ለ፡፡ 4 ፲፡	& F & & O .	120 20 45 1	2118 20 20	35,35,7	339999 34999 34999	TOTAL

NUMMER OF MISSING DAYS OF RECORD EXCEEDED 20% OF YEAR

NOTE:

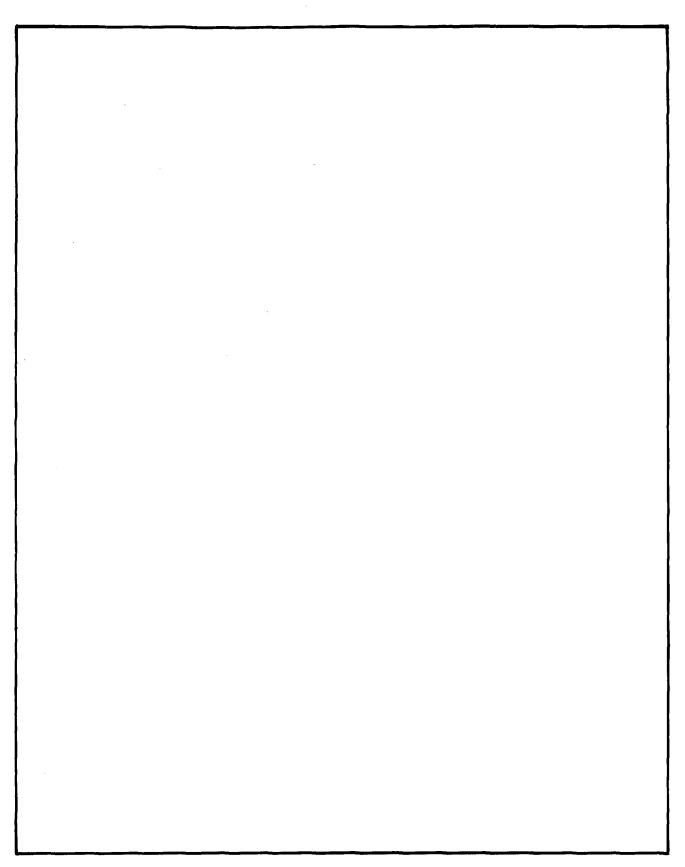


Exhibit B Additional Testing

## ■■ Exhibit B ■■ ADDITIONAL TESTING

It was concluded from Task 1, Well Drilling Program, that no significant groundwater supply exists in the Eagle River Valley. Emphasis was then placed on the study of Eagle River surface water as a potential means to meet the growing water demands of the Municipality of Anchorage. To supplement the data presented in this report for Task 3, Flour Water Treatment Study, samples of water were taken from eight sites along the Eagle River between January and June 1981 and were tested for quality. This Exhibit contains the data from this supplemental testing.

The water sampling sites are shown on Figure B-1. Site A, Eagle River 200 Feet Upstream of Glenn Highway, Right Bank, corresponds to the Task 3 testing site. Other sites were chosen at various points to identify potential contamination sources.

Coliform tests were performed on samples from all the sites; however samples from Sites C and E were not tested on a regular basis. The results of these tests are shown in Table B-1.

Complete State of Alaska drinking water standard tests were performed on water from Sites A and D on a regular basis, and from Sites E and H less frequently. The results of these tests are summarized in Tables B-2 and B-3.

Analysis of the results of the additional testing indicates that the Eagle River surface water should be suitable for human consumption if the proper treatment is applied to it. If this water is selected as a future drinking water source, it is recommended that further, more detailed water quality tests be conducted.

Additionally, there are indications that groundwater is moving from the vicinity of the old Eagle River dump to the river. If the lower damsite (see Appendix II) is chosen for development, the potential impacts of the old dump on the river should be thoroughly analyzed.

Figure B-1 Sampling Sites for Additional Tests

Table B-1 COLIFORM ANALYSIS JANUARY THROUGH JUNE 1981

Site <sup>a</sup>	Date	Fecal Coliform	Total Coliform
Site A	01/22/81 02/24/81 03/19/81 04/01/81 04/08/81 04/22/81 05/15/81 06/23/81	0 2 0 0 11	9 33 TNTCb 2 6 TNTC 2 TNTC
Site B	04/01/81 04/08/81 04/22/81 05/15/81 06/23/81	2 1 3 1 25	3 17 11 0 TNTC
Site C	03/19/81		52
Site D	03/19/81 04/08/81 04/22/81 05/15/81 06/23/81	0 17 0 400	TNTC 5 TNTC TNTC TNTC
Site E	02/24/81 04/01/81	0	4 0
Site F	04/01/81 04/08/81 05/15/81 06/23/81	1 1 0 28	4 18 2 TNTC
Site G	04/01/81 04/08/81 04/22/81 05/15/81 06/23/81	32 1 3 0 54	35 0 TNTC 10 TNTC
Site H	04/01/81 04/08/81 04/22/81 05/15/81	8 2 0 0	22 31 3 8

<sup>&</sup>lt;sup>a</sup>Refer to Figure B-1 for description of sites.

bToo numerous to count.

Table B-2 INORGANICS JANUARY THROUGH JUNE 1981

<u>Site</u> <sup>a</sup>	Date	As	Ba	Cd	Cr	<u>_</u> F	_Fe_	Pb	<u> Mn</u>	Hg	Nitrate-N	_ <u>Se</u> _	Ag	Na
Site A	01/22/81	~ 0.01	<0.5	< 0.010	< 0.01	< 0.1	0.11	<0.01		< 0.001	0.86		< 0.01	2.7
	02/24/81	~ 0.01	<0.5	< 0.010	< 0.01	< 0.1	0.12	< 0.01	0.03	< 0.001	0.62	< 0.01	< 0.01	2.9
	03/19/81	< 0.01	< 0.5	< 0.010	< 0.01	< 0.1	0.50	< 0.01	0.04	< 0.001	0.38	< 0.01	< 0.01	2.5
	04/22/81	< 0.01	< 0.5	< 0.010	< 0.01	< 0.1	0.68	< 0.01	0.07	< 0.001	0.86	< 0.01	< 0.01	2.9
	05/15/81	< 0.01	0.013	< 0.010	< 0.01	< 0.1	0.21	< 0.01	0.02	< 0.001	0.90	< 0.01	< 0.01	2.9
	06/23/81	< 0.01	<b>√0.5</b>	< 0.010	< 0.05	< 0.1	1.6	< 0.01	0.04	< 0.001	0.21	< 0.01	< 0.01	1.7
Site D	03/19/81	< 0.01	<0.5	< 0.010	< 0.01	0.23	8.9	< 0.01	1.0	< 0.001	0.15	< 0.01	< 0.01	2.9
	04/22/81	0.01	< 0.5	< 0.010	< 0.01	< 0.1	2.5	< 0.01	0.20	< 0.001	0.17	< 0.01	< 0.01	3.0
	05/15/81	< 0.01	<b>&lt;0.5</b>	< 0.010	< 0.01	< 0.1	0.88	< 0.01	0.06	< 0.001	0.29	< 0.01	< 0.01	3.7
	06/23/81	< 0.01	<0.5	< 0.010	< 0.01	< 0.1	0.1	< 0.01	< 0.01	< 0.001	0.17	< 0.01	< 0.01	4.2
Site E	02/24/81	< 0.01	<0.5	<0.010	< 0.01	< 0.1	0.13	< 0.01	0.03	< 0.001	0.60	< 0.01	< 0.01	3.3
Site H	04/22/81	< 0.01	< 0.5	< 0.010	< 0.01	< 0.1	0.34	< 0.01	0.02	< 0.001	0.42	< 0.01	< 0.01	3.0

<sup>&</sup>lt;sup>a</sup>Refer to Figure B-1 for site descriptions.

Table B-3 COLOR, TURBIDITY, ORGANICS, AND RADIOACTIVITY JANUARY THROUGH JUNE 1981

					Organics						Radioactivity			
Sitea	<u>Da te</u>	Color	Turbid- ity	<u>Endrin</u>	Lindane	Methox- ychlor	Toxa- phene	2,4D	2,4,5-TP Silvex	Gross A	Cross B	Lab <sup>b</sup>		
Site A	01/22/81 02/24/81 03/19/81 04/22/81 05/15/81 06/23/81	5.0 10.0 20.0 15.0 20.0 20.0	0.55 0.44 4.2 4.8 2.3	< 0.0002 < 0.0002 < 0.0002 < 0.0002 < 0.0002 < 0.0002	<0.004 <0.004 <0.004 <0.004 <0.004 <0.004	< 0.1 < 0.01 < 0.1 < 0.1 < 0.1 < 0.1	< 0.005 < 0.005 < 0.005 < 0.005 < 0.005 < 0.005	< 0.1 < 0.01 < 0.1 < 0.1 < 0.1 < 0.1	<0.01 <0.01 <0.01 <0.01 <0.01 <0.01	9.0 ± 1.0 7.2 ± 1.0 6.2 ± 1.3 0.2 ± 1.2 7.5 ± 2.3 0.0 ± 0.9	4.5 ± 1.1 8.1 ± 1.3 1.8 ± 4.7 2.9 ± 4.3	Chem. & Geo. Chem. & Geo. Chem. & Geo. CH2M HILL Chem. & Geo. CH2M HILL		
Site D	03/19/81 04/22/81 05/15/81 06/23/81	150.0 15.0 70.0 10.0	64.0 26.0 39.0 0.6	< 0.0002 < 0.0002 < 0.0002 < 0.0002	<0.004 <0.004 <0.004 <0.004	< 0.1 < 0.1 < 0.1 < 0.1	< 0.005 < 0.005 < 0.005 < 0.005	< 0.1 < 0.1 < 0.1 < 0.1	<0.01 <0.01 <0.01 <0.01	1.8 ± 0.6 6.4 ± 0.9 4.5 ± 2.1 0.0 ± 1.3	2.1 <u>+</u> 5.3	Chem. & Geo. Chem. & Geo. Chem. & Geo. CH2M HILL		
Site E	02/24/81	10.0	2.5	< 0.0002	<0.004	< 0.1	< 0.005	< 0.1	<0.01	8.1 <u>+</u> 1.3	11.7 ± 1.5	Chem. ۵ Geo.		
Site H	04/22/81 05/15/81	5.0	2.3	< 0.0002	<0.004	< 0.1	< 0.005	< 0.1	<0.01	-0.9 ± 2 -0.1 ± 0.8	4.5 ± 5.0 -0.5 ± 3.6	CH2M HILL CH2M HILL		

<sup>&</sup>lt;sup>a</sup>Refer to Figure B-1 for site descriptions.

<sup>&</sup>lt;sup>b</sup>The reliability of the tests performed by a laboratory in Wyoming for Chemical and Ceological Laboratories of Alaska, Inc., is questionable.

